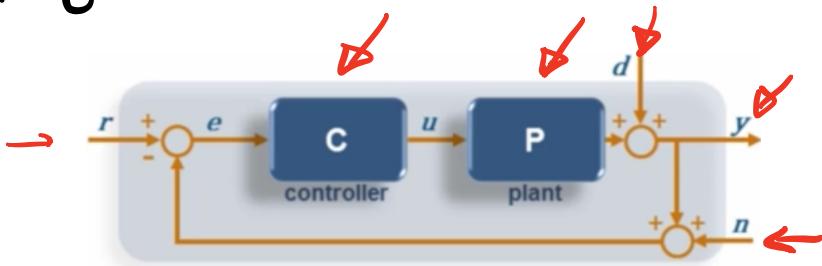


LOOP SHAPING

"shaping the open loop transfer function"



$L = PC$
open loop
transfer
function

Closed Loop Transfer Functions:

$$y = \frac{PC}{(1 + PC)}(r - n) + \frac{1}{(1 + PC)}d$$

T complementary sensitivity **S** sensitivity

$$e = \frac{1}{(1 + PC)}(r - d - n)$$

$T = \frac{PC}{1 + PC}$
Complementary
Sensitivity

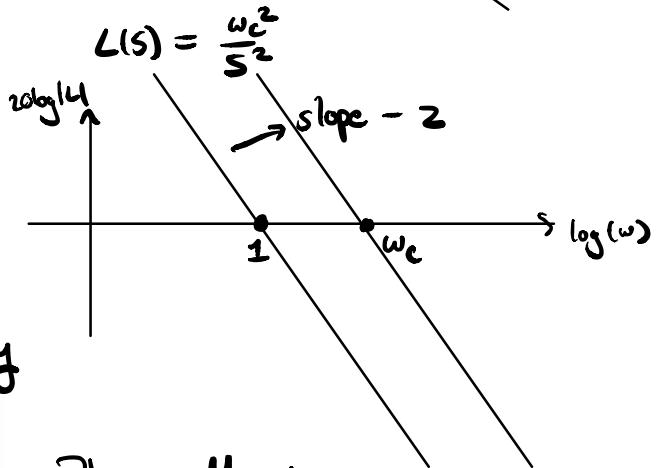
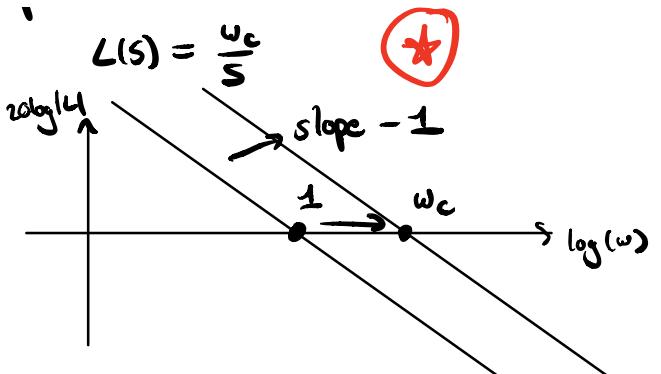
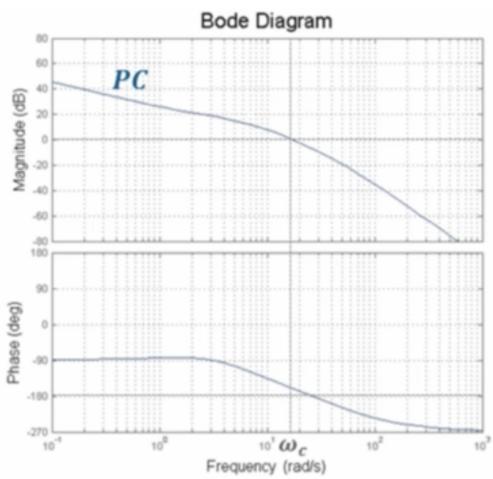
$S = \frac{1}{1 + PC}$ ↗
sensitivity

$$S + T = 1$$

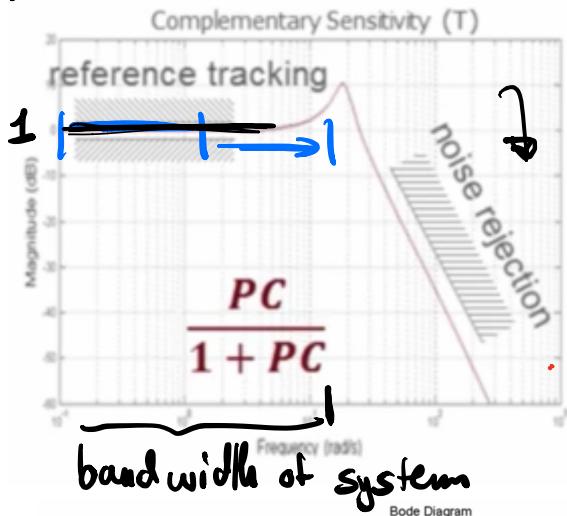
$$y = PCR \quad \text{why not just set } C = P^{-1} \Rightarrow y = r$$

- if denominator of P is higher order than the numerator
 $C = P^{-1}$ is not proper (not causal)

- if P has RHP zeros, $C = P^{-1}$ won't be stable
- P might not be a perfect model



Reference to output: $r \rightarrow y$

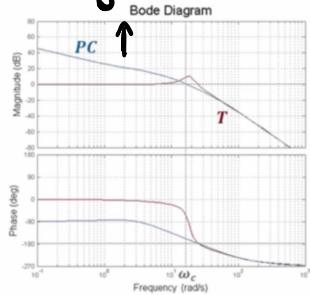


Open Loop vs. T

$$T = \frac{PC}{(1 + PC)}$$

for: $PC \gg 1$
 $T \approx 1$

for: $PC \ll 1$
 $T \approx PC$

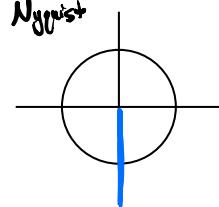


Phase Margin

$$L(s) = \frac{1}{s}$$

$$L(i\omega) = \frac{1}{i\omega} \frac{i}{i} = -i\omega$$

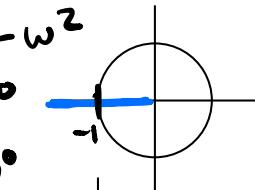
$\Delta L(i\omega) = -90^\circ$ Nyquist
phase margin -90°



$$L(s) = \frac{1}{s^2}$$

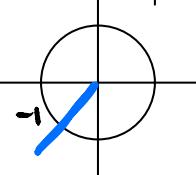
$$L(i\omega) = \frac{1}{i^2\omega^2} = -\omega^2$$

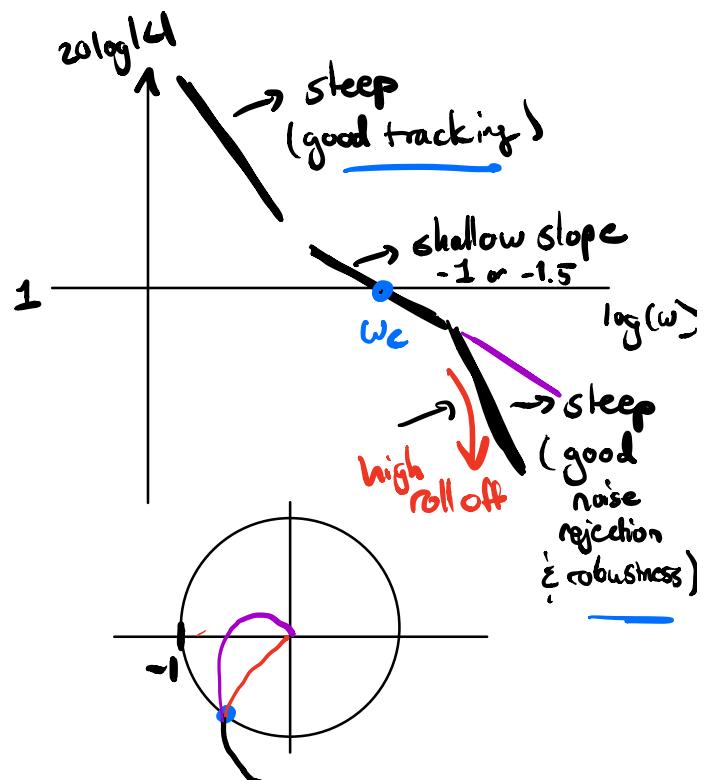
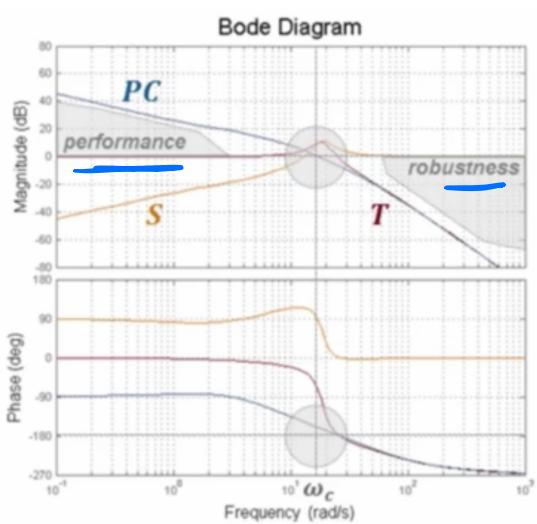
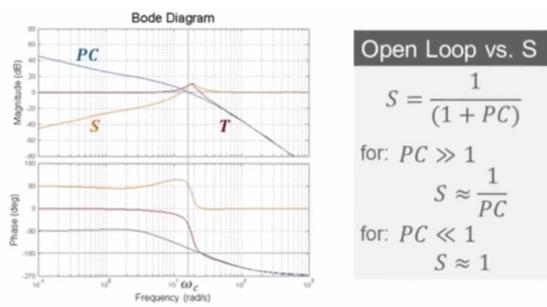
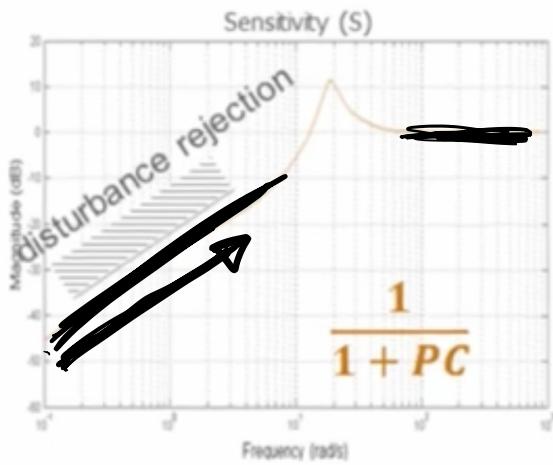
$\Delta L(i\omega) = -180^\circ$
phase margin 0°

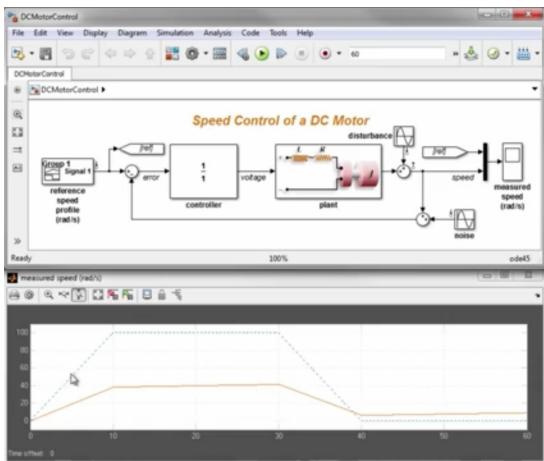


$$L(s) = \frac{1}{s^{1.5}}$$

phase margin -45°







- stability

- zero steady state error

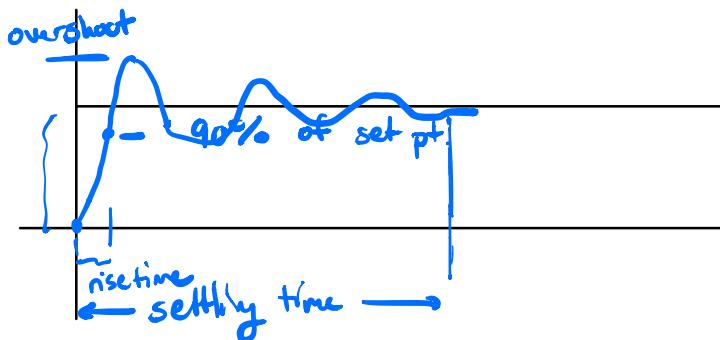
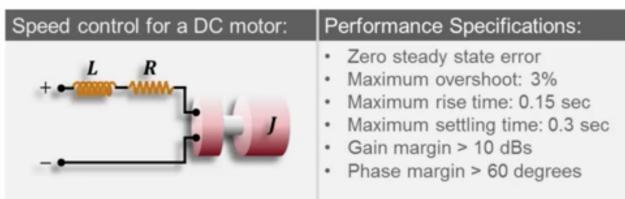
long term

- Max overshoot 3%
- Max rise time 0.15 sec
- Max settling time 0.3 sec

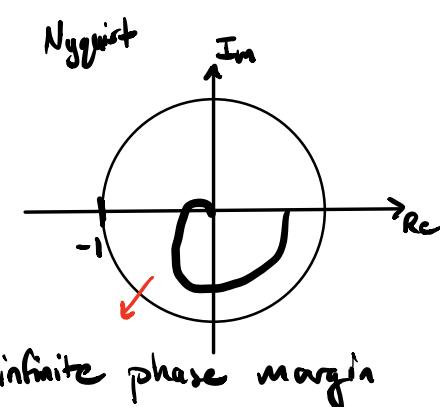
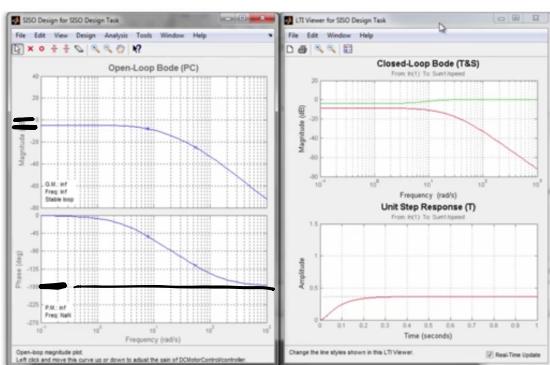
short term
transient

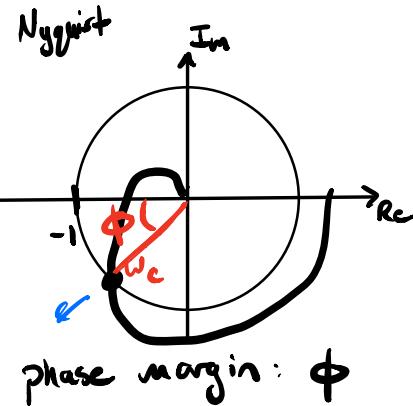
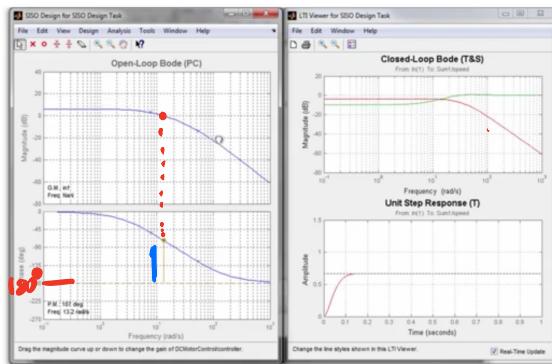
- Gain margin > 10 dBs
- Phase margin > 60 deg

slope of L at
crossover of
 ≈ 1.3

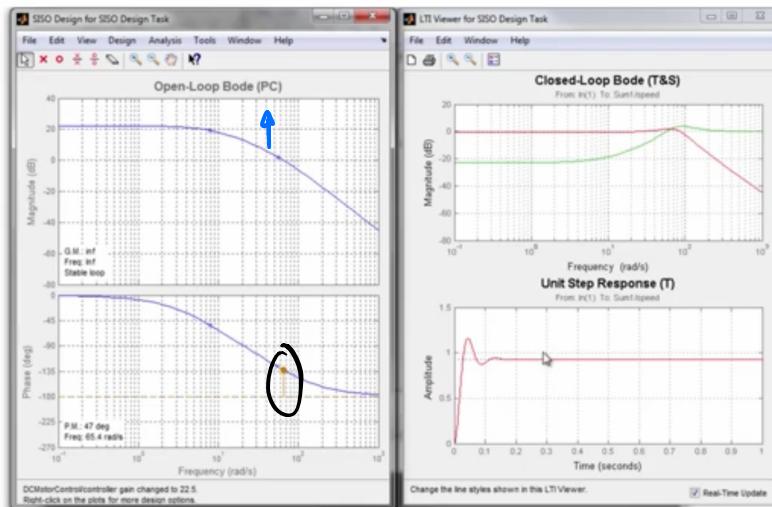


Phase Margin and Transient Specifications

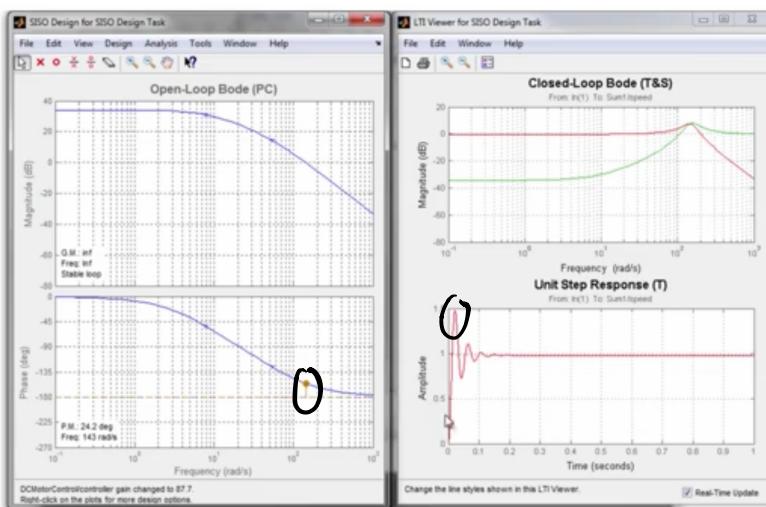




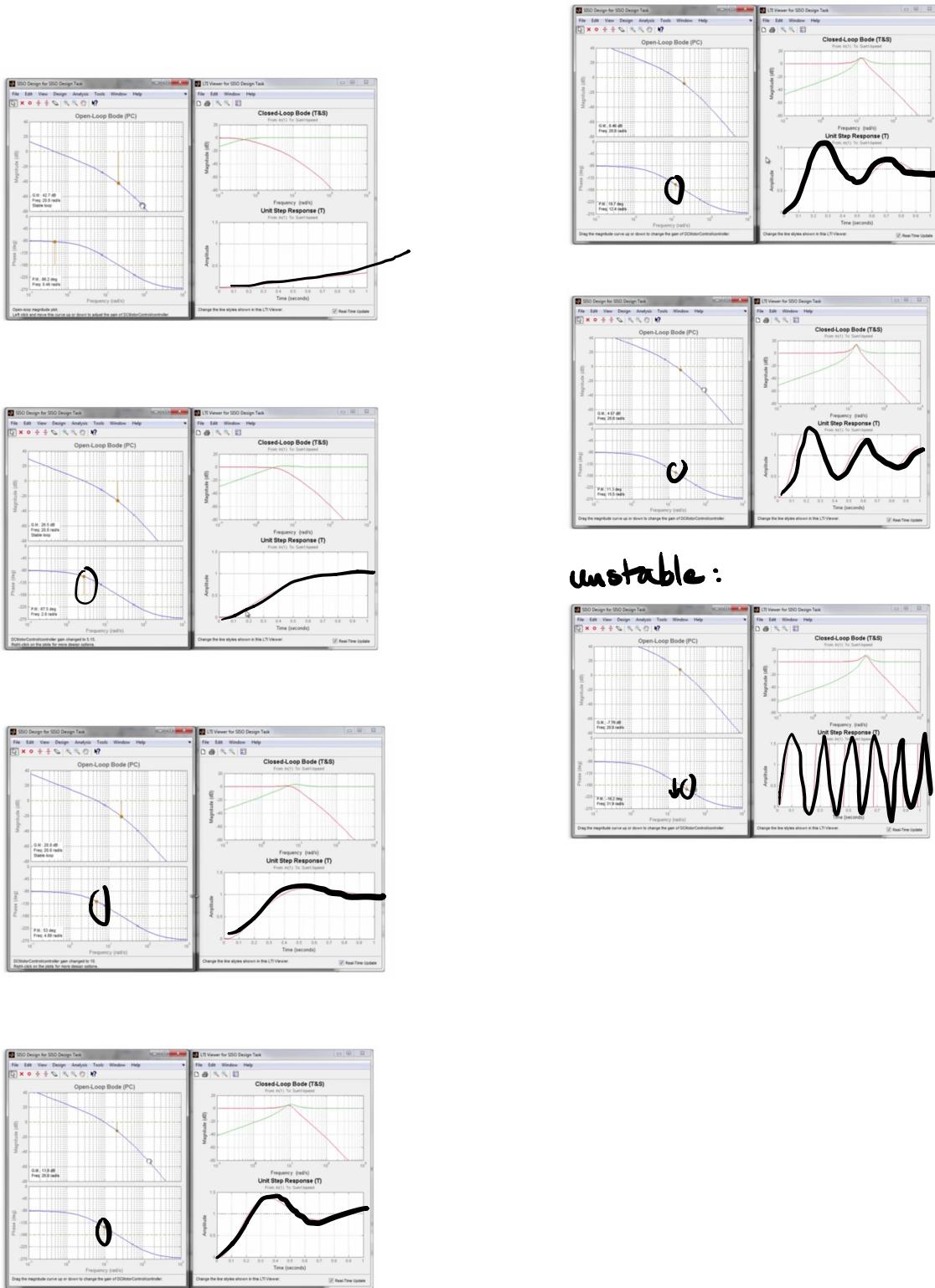
Proportional Controller



Decreased phase margin results in more oscillations
- more overshoot etc.
and if the phase margin goes to 0 the oscillations go out of control ie. the system goes unstable

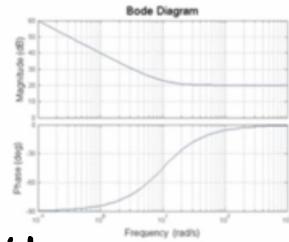


Proportional Integral Controller



Components for Loop Shaping: $C(s) = C_1(s)C_2(s)\dots$

PI Compensator:
drives steady state error to zero, improves disturbance rejection

$$C = K_P + \frac{K_I}{s}$$


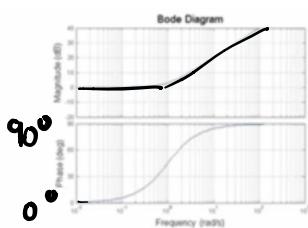
$$k_p + \frac{k_i}{s}$$

$$\frac{k_p s + k_i}{s}$$

$$k_p \left(s + \frac{k_i}{k_p} \right)$$

steeper slope initially.

PI Compensator:
drives steady state error to zero, improves disturbance rejection

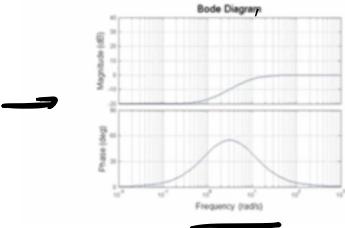
$$C = G_0 \left(\frac{s + \omega_Z}{s} \right)$$


PD Compensator:
 $C = K_P + K_D s$
adds phase lead, improves phase margin, improves damping, speeds up response

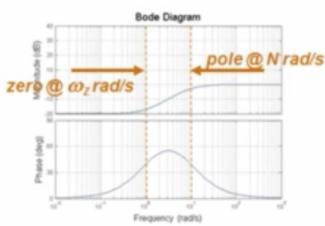
PI compensator:
- integrator initial region
- constant final region

PD Compensators:
aren't proper
not a realizable controller.

this is proper



PD Compensator:
 $C = K_P + \frac{K_D s}{s + N}$
adds phase lead, improves phase margin, improves damping, speeds up response



PD Compensator:
 $C = G_0 \left(\frac{s + \omega_Z}{s + N} \right)$
adds phase lead, improves phase margin, improves damping, speeds up response

Lead Compensator:

adds phase lead,
improves phase margin, improves damping, speeds up response

$$C = \frac{s + 10}{s + 100}$$

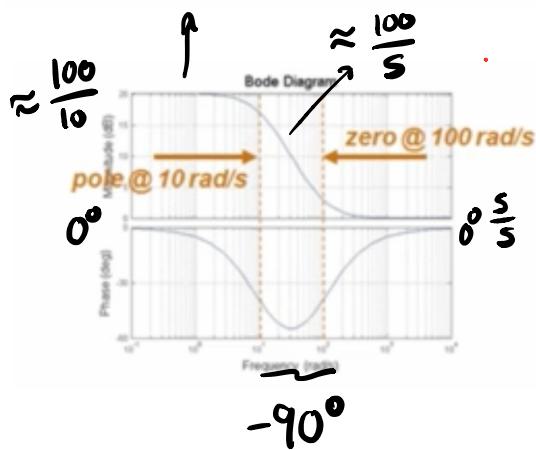
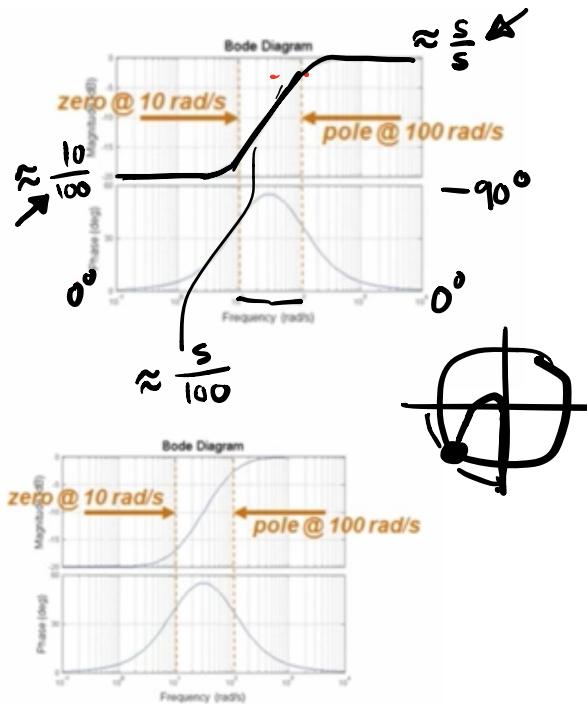
act like PD controllers

Lead Compensator:

adds phase lead,
improves phase margin, improves damping, speeds up response

$$C = \frac{10(0.1s + 1)}{100(0.01s + 1)}$$

$\approx -90^\circ$

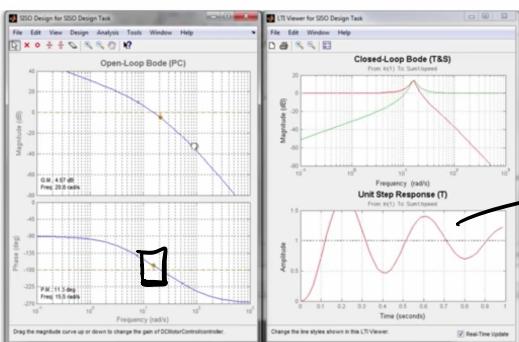


Lag Compensator:

$$C = \frac{s + 100}{s + 10}$$

adds phase lag,
improves disturbance rejection, slows down response

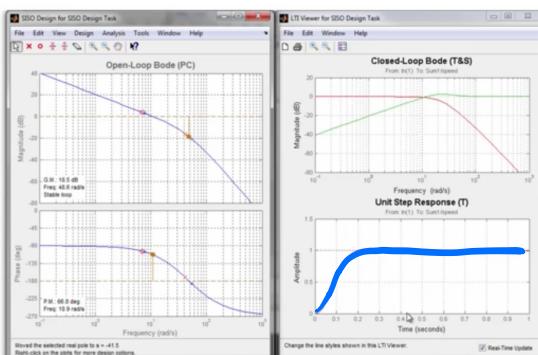
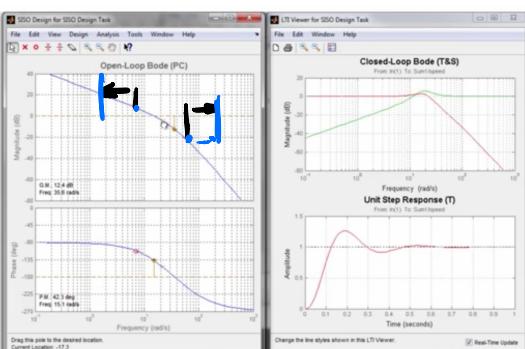
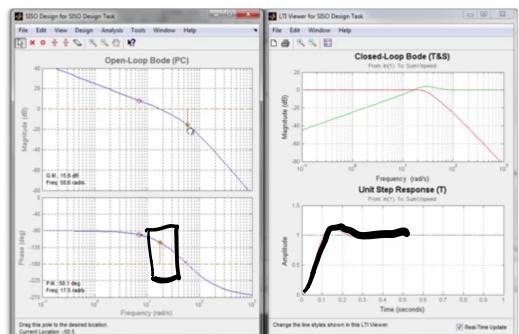
- increase magnitude of L in the tracking region w/out affecting mag in later region
(good tracking and disturbance rejection)



PI Controller \bar{w}
small phase margin

lots of oscillation.

Add a lead compensator



Ex.

$$C(s) = G_0 \left(\frac{s + \omega_2}{s} \right) \left(\frac{s + \omega_1}{s + \omega_2} \right)$$

constant gain PI compensator Lead compensator

