

Connections TF and State space

$$\text{state space: } \begin{aligned} \dot{x} &= Ax + Bu \\ y &= Cx + Du \end{aligned}$$

$$\begin{aligned} \rightarrow sX(s) &= AX + BU \rightarrow X = (sI - A)^{-1}BU \\ Y &= CX + DU \rightarrow Y = [C(sI - A)^{-1}B + D]U \end{aligned}$$

$$\text{TF: } \begin{array}{ccc} U(s) & \longrightarrow & \boxed{G(s)} \longrightarrow Y(s) \end{array}$$

$$G(s) = [C(sI - A)^{-1}B + D]$$

TF to state space:

- multiple state space models
- transfer function determines the minimum # of states in the state space, but could be more states

want a state space with the minimum number of states \rightarrow minimal realization

$$G(s) = \frac{\beta_{n-1}s^{\overset{n-1}{\circ}} + \dots + \beta_1s + \beta_0}{s^n + \alpha_{n-1}s^{n-1} + \dots + \alpha_1s + \alpha_0} \leftarrow$$

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

where

$$A = \begin{bmatrix} 0 & 1 & & 0 \\ \vdots & & \ddots & \\ 0 & 0 & & 1 \\ -\alpha_0 & -\alpha_1 & \dots & -\alpha_{n-1} \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

Canonical
minimal
realization

$$C = [B_0 \dots B_{n-1}] \quad D = \boxed{0}$$

strictly proper transfer function $G(s)$
since the numerator has degree less than
the denominator

if we have a proper trans. function
(not strictly proper), i.e. the degree of the
numerator is equal to degree of denominator

$$G(s) = C(sI - A)^{-1}B + D \leftarrow \text{constant}$$

$$(sI - A)^{-1} = \frac{1}{\det(sI - A)} \begin{bmatrix} \text{Adj}(sI - A) \end{bmatrix}$$

$A \in \mathbb{R}^{n \times n}$

denominator
of $G(s)$

Adjugate
matrix

↪ ea. term is
a determinant of
a submatrix

all terms only go
up to degree $n-1$

$$G(s) = \frac{C \overbrace{\text{Adj}(sI - A)}^{n-1 \text{ deg. poly.}} B + D \overbrace{\det(sI - A)}^{n \text{ deg. poly.}}}{\det(sI - A)}$$

for proper (not strictly proper) TF:

$$G(s) = \frac{\beta_n s^n + \dots + \beta_1 s + \beta_0}{s^n + \alpha_{n-1} s^{n-1} + \dots + \alpha_1 s + \alpha_0}$$

Minimal Realization:

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

where

$$A = \begin{bmatrix} 0 & 1 & & 0 \\ \vdots & & \ddots & \\ 0 & 0 & & 1 \\ -\alpha_0 & -\alpha_1 & & -\alpha_{n-1} \end{bmatrix}$$

$$B = \begin{bmatrix} 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

$$C = [\beta_0 - \alpha_0 \beta_n, \beta_1 - \alpha_1 \beta_n, \dots, \beta_{n-1} - \alpha_{n-1} \beta_n] \quad D = \beta_n$$

C here is the previous C + $\det(sI - A)D$

Intuitively:

$$x = \begin{bmatrix} z \\ \dot{z} \\ \ddot{z} \\ \vdots \\ z^{(n-1)} \\ z \end{bmatrix} \quad \dot{x} = \begin{bmatrix} \dot{z} \\ \ddot{z} \\ \vdots \\ z \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & 1 \\ -\alpha_0 & -\alpha_1 & \dots & \dots & -\alpha_{n-1} \end{bmatrix} \begin{bmatrix} z \\ \dot{z} \\ \ddot{z} \\ \vdots \\ z \end{bmatrix} + Bu$$

Stability: $\text{eig}(A) \in \text{OLHP}$ $\text{eig}(A)$

if degree of numerator of $G(s)$ greater than denominator \rightarrow improper TF.

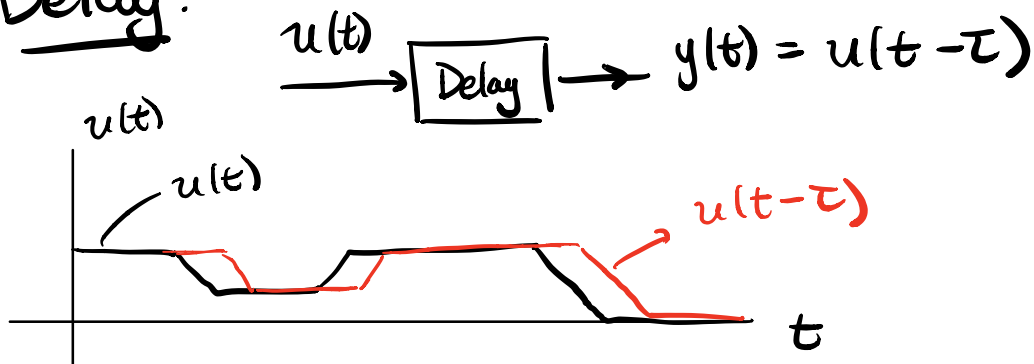
\rightarrow no physical system would give this TF
 \rightarrow violates causality.

Stability Assessment:

so far:

- Routh Hurwitz
- Eigenvalues of sys matrix.
- Nyquist Criteria. } \rightarrow allow us to model delays

Delay:



Laplace transform

$$Y(s) = e^{-\tau s} U(s)$$

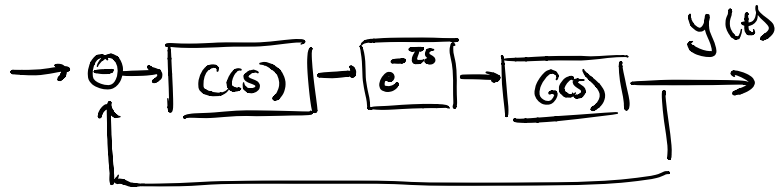
$$|e^{-\tau i\omega}| = 1$$

time delay doesn't change the magnitude

$$\angle e^{-\tau i\omega} = -\tau\omega$$

shifts the phase of the signal by $-\tau\omega$

Before :



open loop
TF

$$L(s) = e^{-Ts} C(s) G(s)$$

char
eqn

$$1 + L(s) = 0 \Rightarrow 1 + \underbrace{e^{-Ts} C(s) G(s)}_{\text{roots?}} = 0$$

Ex. PD control of a car.

$$C(s) = k_p + k_d s \quad G(s) = \frac{1}{ms^2}$$

$$1 + L(s) = 1 + e^{-Ts} \left(\frac{k_p + k_d s}{ms^2} \right) = 0$$

$$\underline{ms^2 + e^{-Ts} (k_p + k_d s)} = 0$$

infinite degree polynomial

$$e^{-Ts} = 1 - Ts + \frac{(-Ts)^2}{2} + \frac{(-Ts)^3}{3!} + \dots$$

Taylor
Expansion
of e^{-Ts}

$$\underline{ms^2 + e^{-Ts} (k_p + k_d s)} = 0 \rightarrow \text{infinite number of roots.}$$

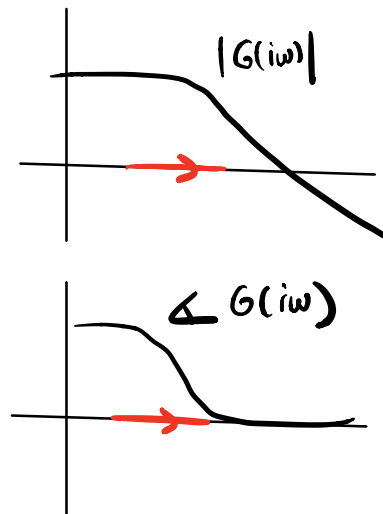
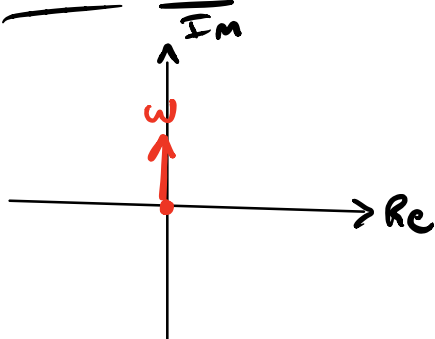
any state space model

\rightarrow infinite # of states.

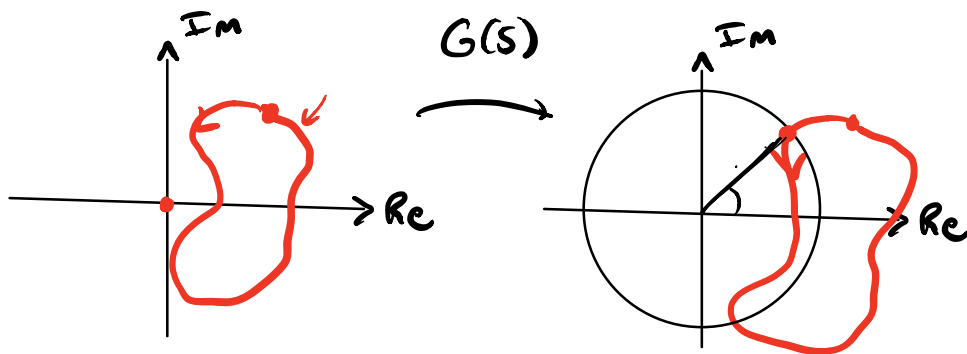
Nyquist Plots

another way to analyze TF

Bode Plot:

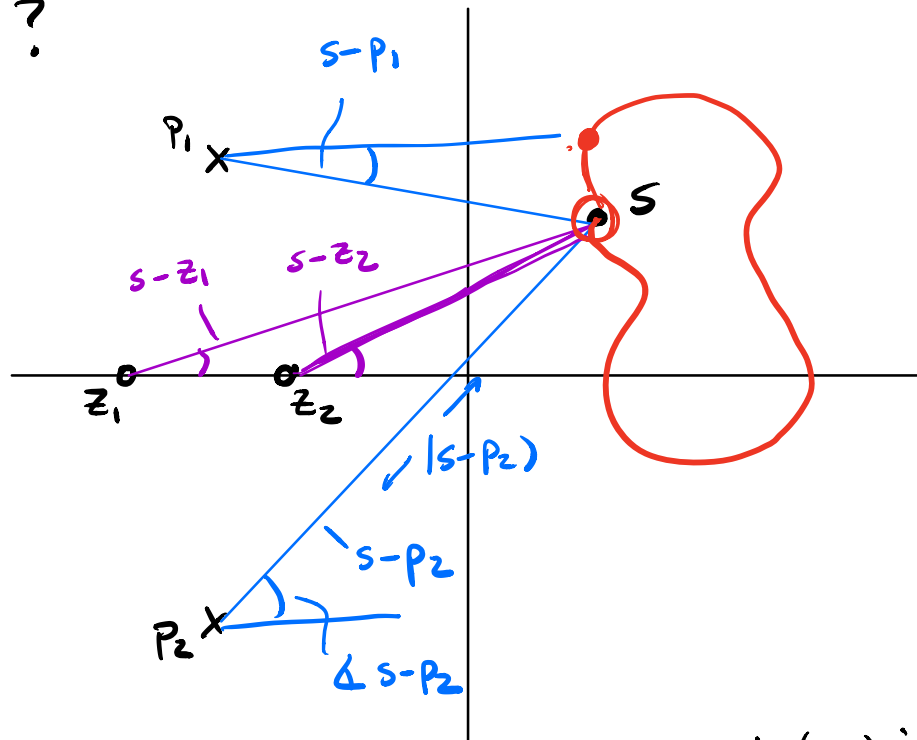


Nyquist Plot



$$G(s) = \frac{(s-z_1) \cdots (s-z_l)}{(s-p_1) \cdots (s-p_n)}$$

$$G(s) = ?$$

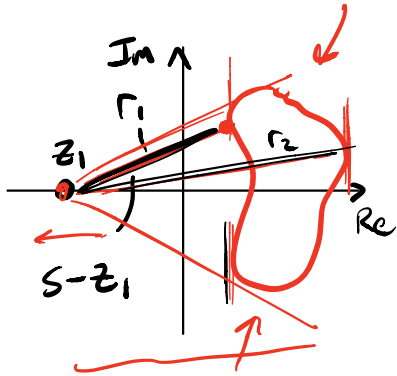


$$G(s) = \frac{(s-z_1)(s-z_2)}{(s-p_1)(s-p_2)} = \frac{|s-z_1||s-z_2| e^{i\Delta(s-z_1)} e^{i\Delta(s-z_2)}}{|s-p_1||s-p_2| e^{i\Delta(s-p_1)} e^{i\Delta(s-p_2)}}$$

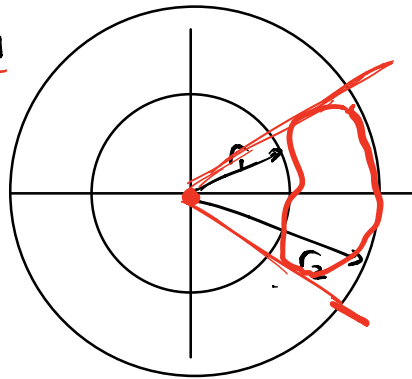
$$= \frac{|s-z_1||s-z_2|}{|s-p_1||s-p_2|} e^{\Delta(s-z_1) + \Delta(s-z_2) - \Delta(s-p_1) - \Delta(s-p_2)}$$

in general:

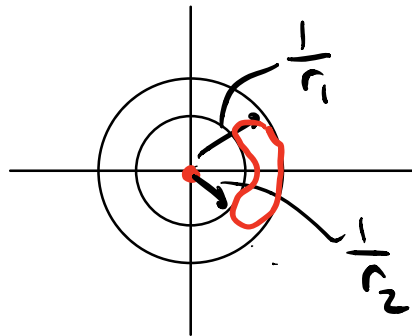
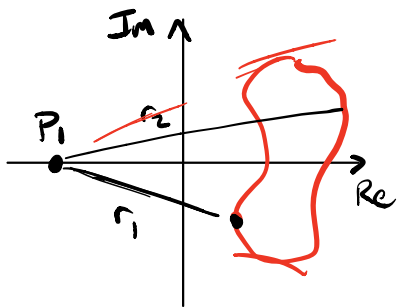
$$G(s) = \frac{\prod_k |s-z_k|}{\prod_{k'} |s-p_{k'}|} e^{i \sum_k \Delta(s-z_k) - i \sum_{k'} \Delta(s-p_{k'})}$$



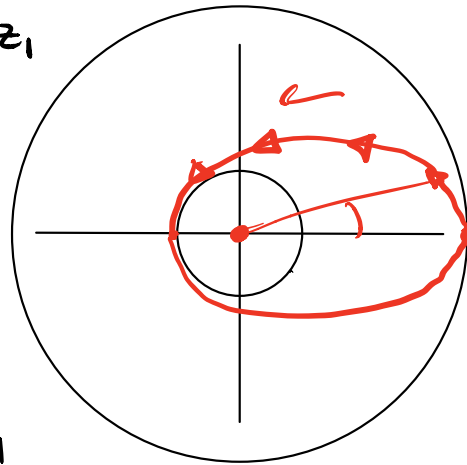
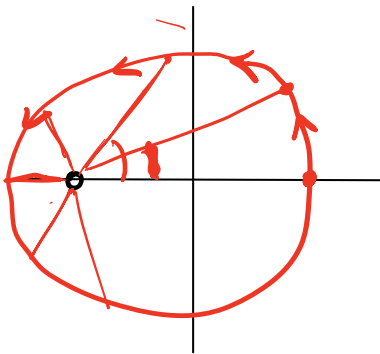
$$G(s) = s - z_1$$



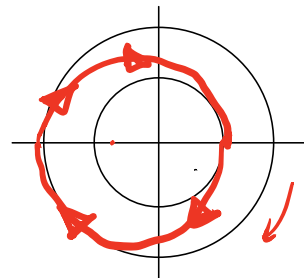
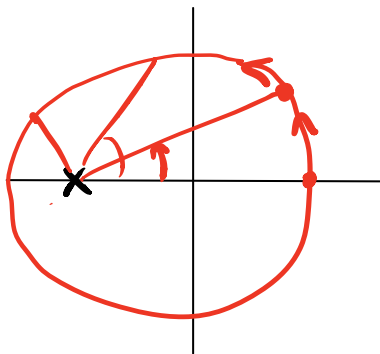
$$G(s) = \frac{1}{s - p_1}$$



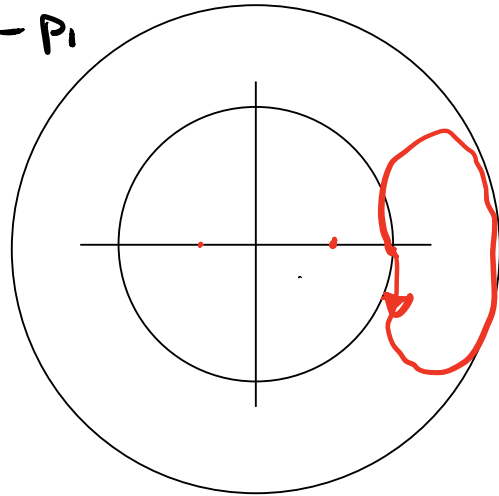
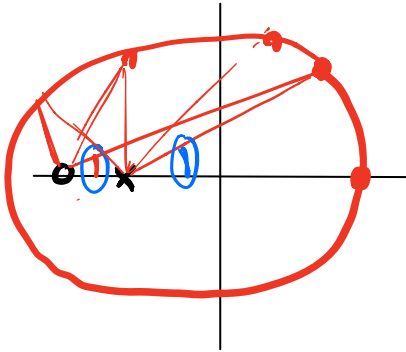
$$G(s) = s - z_1$$



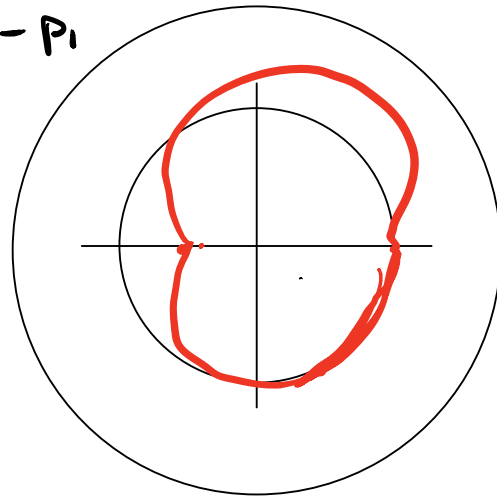
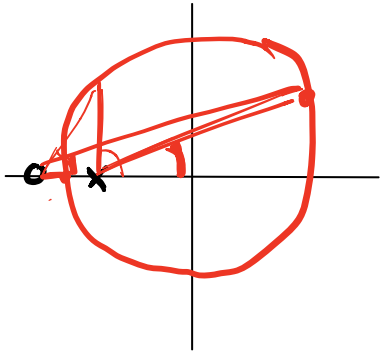
$$G(s) = \frac{1}{s - p_1}$$



$$G(s) = \frac{s - z_1}{s - p_1}$$



$$G(s) = \frac{s - z_1}{s - p_1}$$



phase of $s - p_1$

0 all the way to 360

phase of $s - z_1$

45° and -45°

Cauchy Argument Principle:

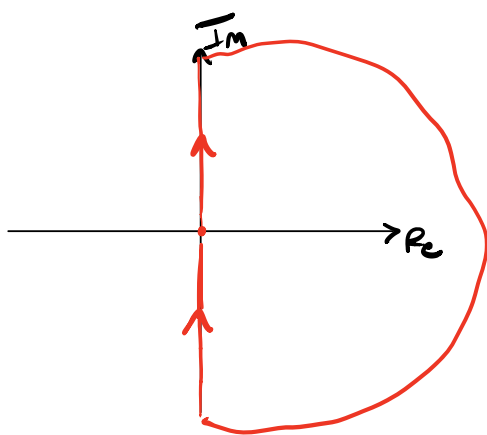
For a complex rational function $G(s)$

$$\# \text{ zeros inside a contour} = \# \text{ CW encirclements of origin} + \# \text{ of poles inside a contour}$$

or

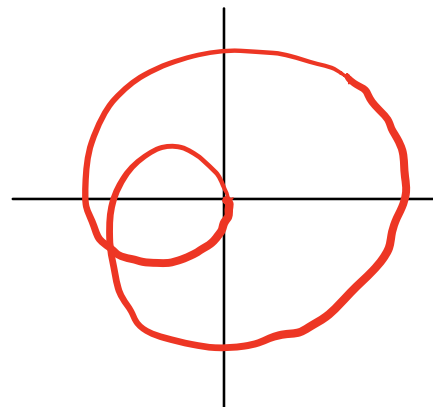
$$\# \text{ zeros inside a contour} - \# \text{ of poles inside a contour} = \# \text{ CW encirclements of origin}$$

Nyquist Contour \rightarrow encloses the RHP



$1+L(s)$
 $\xrightarrow{\hspace{2cm}}$

Nyquist Plot:



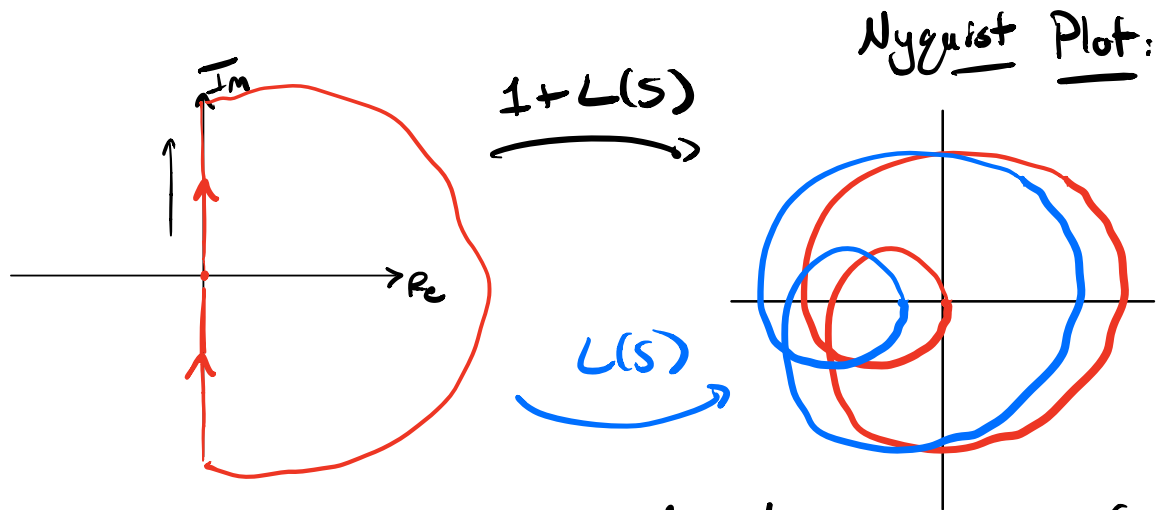
For stability:

interested in zeros

$$1+L(s) = 0$$

$$L(s) = C(s)G(s)$$

count encirclements
of the origin



we can understand the zeros of $1+L(s)$ by counting the number of times that $L(s)$ encircles -1 in the Nyquist plot.

$$G(s) = \frac{\text{num}_G}{\text{den}_G} \quad C(s) = \frac{\text{num}_C}{\text{den}_C}$$

$$1 + L(s) = 1 + G(s)C(s) = 1 + \frac{\text{num}_G}{\text{den}_G} \frac{\text{num}_C}{\text{den}_C}$$

$$\underbrace{\hspace{1.5cm}}_{\text{roots are zeros}} = \frac{\text{den}_C \text{den}_G + \text{num}_G \text{num}_C}{\text{den}_G \text{den}_C} \rightarrow \text{poles}$$

- Draw Nyquist plot of $L(s)$
- count # of CW encirclements of -1

- know
 → # RHP zeros = # CW encirclements of -1 + # RHP poles

want none in RHP roots of $1 + L(s)$
 want this to be 0
 RHP poles of $L(s)$
 roots of $\text{den}_g \text{den}_c$
 know this

Want

- # CW encirclements of -1 = # RHP poles of $L(s)$ stability

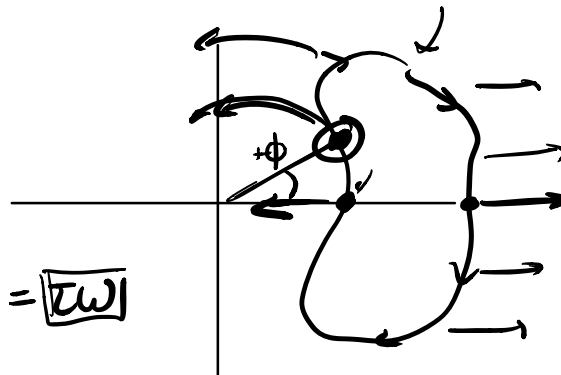
CW encirclements of -1 = # RHP poles of $L(s)$

Nyquist Stability Criterion

Time delay:

$$\frac{L(s)e^{-Ts}}{e^{-i\phi}}$$

$\phi = |\tau\omega|$



$$L(s) + \boxed{1}$$