

AE 513 - Multivariable Control - Autumn 2019

Homework 5

Due Date: Friday, Nov 8st, 2019 at 11:59pm

1. **Lagrange Multipliers** Use the method of Lagrange multipliers to solve the following optimization problems.

(a) **(PTS: 0-2)**

$$\begin{aligned} \min_{x_1, x_2} \quad & x_1^2 + 2x_2^2 \\ \text{s.t.} \quad & x_1 + x_2 = 1; \end{aligned}$$

(b) **(PTS: 0-2)**

$$\begin{aligned} \min_{x \in \mathbb{R}^3} \quad & x^T Q x + c^T x \\ \text{s.t.} \quad & Ax = b; \end{aligned}$$

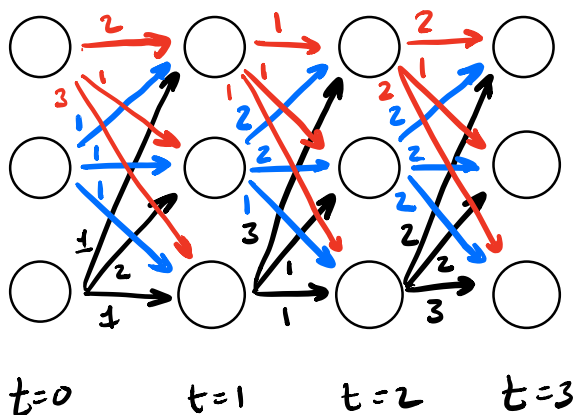
with

$$Q = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 2 & 0 \\ 0 & 0 & 3 \end{bmatrix}, \quad c = \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}, \quad A = \begin{bmatrix} 1 & 2 & -1 \\ 1 & 1 & 0 \end{bmatrix}, \quad b = \begin{bmatrix} -1 \\ 1 \end{bmatrix}$$

2. **Dynamic Programming**

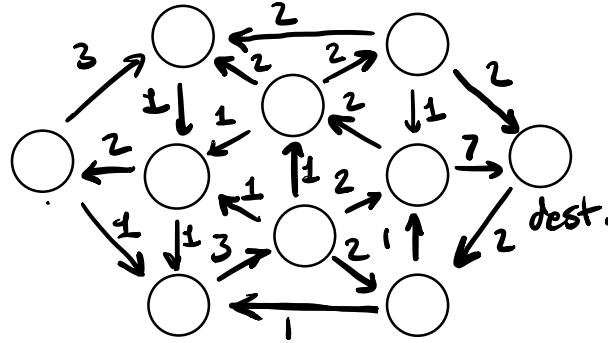
(a) **Finite horizon example:**

(PTS: 0-2) Compute the minimal cost from layer $t = 0$ to layer $t = 3$ for each node by computing the optimal *cost-to-go* or *value* at each node.



(b) **Fixed point example:**

(PTS: 0-2) Consider the graph below. Initialize the *cost-to-go* or *value* at each node at infinity (or some large number). Iterate over each node using the Bellman equation to update the value to reflect the minimum cost-to-go to the destination. (During each update, you should assume that the values at the other nodes accurately reflect the cost-to-go to the destination.) Repeat this process until the value at each node converges.



3. Finite Horizon LQR Extensions

Consider the following extension of the LQR problem in the continuous time case

$$\begin{aligned} \min_{u(t)} \quad & \int_0^T (x - \bar{x})^\top Q(t)(x - \bar{x}) + 2(x - \bar{x})^\top N(t)(u - \bar{u}) + (u - \bar{u})^\top R(t)(u - \bar{u}) dt + \\ & (x(T) - \bar{x}(T))^\top Q(T)(x(T) - \bar{x}(T)) \quad (1) \\ \text{s.t.} \quad & \dot{x} = A(t)x + B(t)u, \quad x(0) = x_0 \quad (2) \end{aligned}$$

The time dependence on x and u are assumed. $\bar{u}(t)$ and $\bar{x}(t)$ are desired control and state trajectories respectively, and $A \in R^{n \times n}$, $B \in R^{n \times m}$, $Q \in R^{n \times n}$, $N \in R^{n \times m}$ and $R \in R^{m \times m}$. The equivalent discrete time problem is given by

$$\begin{aligned} \min_{u(t)} \quad & \sum_{t=0}^{T-1} (x - \bar{x})^\top Q[t](x - \bar{x}) + 2(x - \bar{x})^\top N[t](u - \bar{u}) + (u - \bar{u})^\top R[t](u - \bar{u}) dt + \\ & (x[T] - \bar{x}[T])^\top Q[T](x[T] - \bar{x}(T)) \quad (3) \\ \text{s.t.} \quad & x[t + 1] = A[t]x[t] + B[t]u[t], \quad x[0] = x_0 \quad (4) \end{aligned}$$

(a) In the discrete time case:

- i. (PTS: 0-2) Show that the cost-to-go from time t has the form $(x - \bar{x})^\top P[t](x - \bar{x})$ and derive the Riccati update equation to solve for $P[t]$.
- ii. (PTS: 0-2) Derive the form of the optimal feedback control law.

(b) In the continuous time case:

- i. (PTS: 0-2) Show that the cost-to-go from time t has the form $(x - \bar{x})^\top P(t)(x - \bar{x})$ and derive the Riccati differential equation to solve for $P(t)$.
- ii. (PTS: 0-2) Derive the form of the optimal feedback control law.

4. Infinite Horizon LQR

The *infinite horizon continuous time LQR problem* is given by

$$\min_{u(t)} \int_0^{\infty} x^T Q x + u^T R u \, dt \quad (5)$$

$$\text{s.t. } \dot{x} = Ax + Bu, \quad x(0) = x_0 \quad (6)$$

For a long time horizon, the cost-to-go matrix P converges, ie. \dot{P} goes to 0 and can be found by solving the *algebraic Riccati equation*

$$0 = A^T P + PA + Q - PBR^{-1}B^T P$$

with optimal gains given by

$$K = -R^{-1}B^T P$$

Let $x \in R^3$ and

$$A = \begin{bmatrix} 1 & 2 & 3 \\ 2 & -1 & -1 \\ 2 & 2 & 1 \end{bmatrix}, \quad B = \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ 0 & 0 \end{bmatrix},$$

Select $Q = Q^T \geq 0$ and $R = R^T > 0$.

(PTS: 0-2) Solve the Riccati differential equation

$$-\dot{P} = A^T P + PA + Q - PBR^{-1}B^T P$$

from the terminal condition $P(T) = Q$.

(PTS: 0-2) Demonstrate that as P progresses backwards in time it converges to the solution to the algebraic Riccati equation. (You can solve the algebraic Riccati equation using the `lqr` function in MATLAB.)

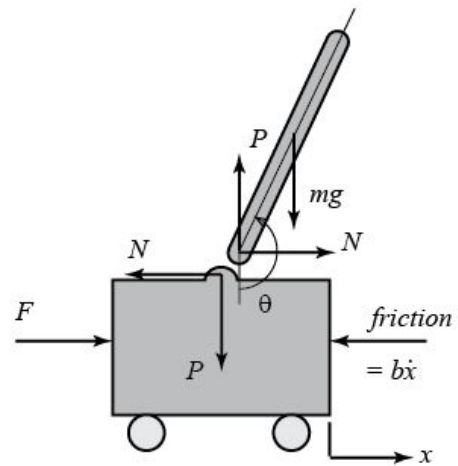
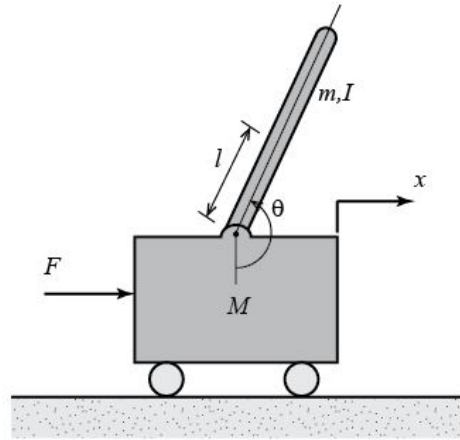
5. LQR Design

For the two systems given below perform the following steps. You can use either discrete or continuous time.

- (PTS: 0-2)** Set $Q = C^T C$ and pick R . Compute an infinite horizon LQR controller.
- (PTS: 0-2)** Compute a finite horizon LQR controller.
- (PTS: 0-2)** Simulate the system from several initial conditions for the two different controllers and compare.
- (PTS: 0-2)** For the infinite horizon controller, modify Q to penalize different states. Try several cases. Recompute the optimal controller in each case. (You can use the `lqr` command.) Simulate the trajectories and compare them.

Systems

1. Inverted Pendulum



System Parameters

- (a) $M =$ mass of cart $0.5 [kg]$
- (b) $m =$ mass of the pendulum $0.2 [kg]$
- (c) $b =$ coefficient of friction for cart $0.1 [N/m/s]$
- (d) $l =$ length of pendulum center of mass $0.3 [m]$
- (e) $I =$ mass moment of inertia of the pendulum $0.006 [kg \cdot m^2]$
- (f) $F =$ force applied to the cart
- (g) $x =$ cart position coordinate
- (h) $\theta =$ pendulum angle from vertical (down)
- (i) $\phi = \theta - \pi$

Equations of Motion (for small θ):

$$l(I + ml^2) \ddot{\phi} - mgl\phi = ml\ddot{x}$$

$$(M + m)\ddot{x} + b\dot{x} - ml\ddot{\phi} = u$$

State-space:

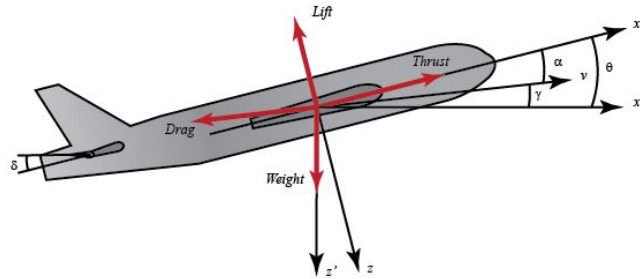
$$\begin{bmatrix} \dot{x} \\ \ddot{x} \\ \dot{\phi} \\ \ddot{\phi} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & \frac{-(I+ml^2)b}{I(M+m)+Mml^2} & \frac{m^2gl^2}{I(M+m)+Mml^2} & 0 \\ 0 & 0 & 0 & 0 \\ 0 & \frac{-mlb}{I(M+m)+Mml^2} & \frac{mgl(M+m)}{I(M+m)+Mml^2} & 0 \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \\ \phi \\ \dot{\phi} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{I+ml^2}{I(M+m)+Mml^2} \\ 0 \\ \frac{ml}{T(M+m)+Mml^2} \end{bmatrix} u$$

$$\mathbf{y} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \\ \phi \\ \dot{\phi} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \end{bmatrix} u$$

$$\begin{bmatrix} \dot{x} \\ \ddot{x} \\ \dot{\phi} \\ \ddot{\phi} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & -0.1818 & 2.6727 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & -0.4545 & 31.1818 & 0 \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \\ \phi \\ \dot{\phi} \end{bmatrix} + \begin{bmatrix} 0 \\ 1.8182 \\ 0 \\ 4.5455 \end{bmatrix} u$$

$$\mathbf{y} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \\ \phi \\ \dot{\phi} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \end{bmatrix} u$$

2. Aircraft Pitch



System Parameters

α = angle of attack

θ = pitch angle

$\mu = \frac{\rho S \bar{c}}{4m}$

S = area of wing

m = aircraft mass

U = equilibrium flight of speed

C_D = Coefficient of Drag

C_W = Coefficient of Weight

γ = Flight path angle

i_{yy} = normalized moment of inertia

q = pitch rate

δ = elevator deflection angle

ρ = air density

\bar{c} = mean chord length

$\Omega = \frac{2U}{\bar{c}}$

C_T = Coefficient of Thrust

C_L = Coefficient of Lift

C_M = Coefficient of Pitch Moment

$\sigma = \frac{1}{1+\mu C_L} = \text{constant}$

$\eta = \mu \sigma C_M = \text{constant}$

Equations of Motion:

$$\begin{aligned}\dot{\alpha} &= \mu\Omega\sigma \left[-(C_L + C_D)\alpha + \frac{1}{(\mu - C_L)}q - (C_W \sin \gamma)\theta + C_L \right] \\ \dot{q} &= \frac{\mu\Omega}{2i_{yy}} [[C_M - \eta(C_L + C_D)]\alpha + [C_M + \sigma C_M(1 - \mu C_L)]q + (\eta C_W \sin \gamma)\delta] \\ \dot{\theta} &= \Omega q\end{aligned}$$

State-space:

$$\begin{aligned}\begin{bmatrix} \dot{\alpha} \\ \dot{q} \\ \dot{\theta} \end{bmatrix} &= \begin{bmatrix} -0.313 & 56.7 & 0 \\ -0.0139 & -0.426 & 0 \\ 0 & 56.7 & 0 \end{bmatrix} \begin{bmatrix} \alpha \\ q \\ \theta \end{bmatrix} + \begin{bmatrix} 0.232 \\ 0.0203 \\ 0 \end{bmatrix} [\delta] \\ y &= \begin{bmatrix} 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \alpha \\ q \\ \theta \end{bmatrix}\end{aligned}$$