

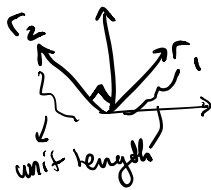
OUTLINE:

- LIN ALG.
- LTI SYSTEMS
- CONTROLLABILITY / OBSERVABILITY
- FEEDBACK CONTROL / OBSERVER DESIGN } → DUAL PROBLEMS

LIN ALG.

SPECIAL MATRICES

- ROTATION MATRICES: $R \in \mathbb{R}^{n \times n}$ $R^T R = I, \det(R) = 1.$



$R = \begin{bmatrix} | & | \\ r_1 & r_2 \\ | & | \end{bmatrix}$ Rotation Matrices
 - orthonormal coordinate systems

- preserve metric properties

$$x = Rz \quad x^T x = z^T R^T R z = z^T z$$

- Symmetric Matrices:

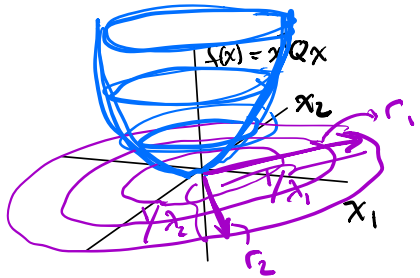
$$Q \in \mathbb{R}^{n \times n} \quad Q = Q^T$$

- have pure real eigen values
- diagonalized by a rotation matrix

$$Q = R D R^T$$

real vals on diag

Quadratic Form:
 $f(x) = x^T Q x \in \mathbb{R}$



Q pos def. or PD

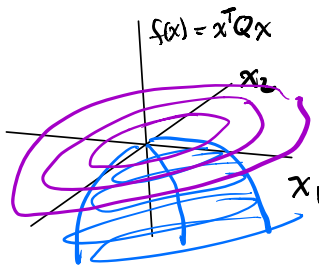
$$x^T Q x > 0 \quad \forall x \rightarrow \lambda_1, \dots, \lambda_n > 0$$

$$x^T R D R^T x \quad R = \begin{bmatrix} | & | \\ r_1 & r_2 \\ | & | \end{bmatrix}$$

rotated coord sys

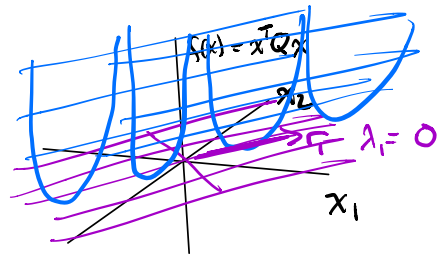
$$r_1^T \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix} \begin{bmatrix} r_1 \\ r_2 \end{bmatrix} r_1$$

$\begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \lambda_1$



Q neg def or ND

$$x^T Q x < 0 \quad \forall x \rightarrow \lambda_1, \dots, \lambda_n < 0$$

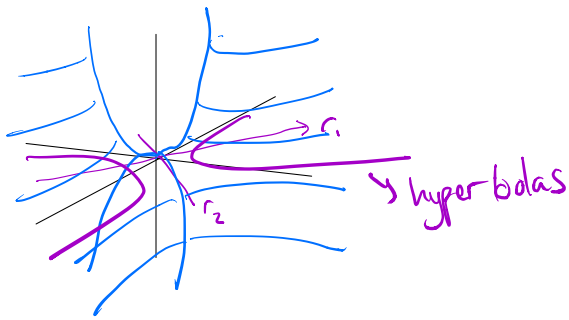


Q pos semi def or PSD

$$x^T Q x \geq 0 \quad \forall x \quad \lambda_1, \dots, \lambda_n \geq 0$$

also neg semi def NSD similar... flipped

$$x^T Q x \leq 0 \quad \forall x \rightarrow \lambda_1, \dots, \lambda_n \leq 0$$



SADDLE FUNCTION

$$\lambda_1, \dots, \lambda_n \geq \text{or} \leq 0$$

worth playing with.

- SKEW SYMMETRIC MATRIX: $K \in \mathbb{R}^{n \times n}$ $K = -K^T$

- pure imaginary eigenvalues \rightarrow the eigen values always come in conjugate pairs

$$K = R \begin{bmatrix} 0 & -b_1 \\ b_1 & 0 \\ & 0 & -b_2 \\ & b_2 & 0 \\ & & & \ddots \end{bmatrix} R^T$$

not a diagonalization but related \rightarrow

related to complex eigenvalues from last week

$$\lambda_1 = b_1 i, \lambda_2 = -b_1 i, \dots$$

\Rightarrow if n is odd at least one $\lambda_i = 0$

- $x^T K x = 0$ for $\forall x \in \mathbb{R}^n \rightarrow$ compute directly

SIDE NOTE: $A = \underbrace{\frac{1}{2}(A+A^T)}_{\text{symmetric}} + \underbrace{\frac{1}{2}(A-A^T)}_{\text{skew symmetric}}$

general matrix $\in \mathbb{R}^{n \times n}$

$$x^T A x = \underbrace{\frac{1}{2} x^T (A+A^T) x}_{\text{sym}} + \underbrace{\frac{1}{2} x^T (A-A^T) x}_0$$

side note:

$$f(x) = x^T Q x$$

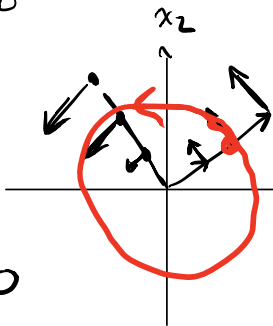
$$\nabla f(x) = 2x^T Q$$

- $\dot{x} = Kx$

2 things • proportional to $|x|$

• $x^T x = 0$

- $x^T K^T x = 0$



skew sym matrices represent "rotational vector fields"

- e^{kt} always a rotation matrix

$$\dot{x} = kx \rightarrow \text{integrate } e^{kt} = R \begin{bmatrix} \cos bt & -\sin bt & 0 \\ \sin bt & \cos bt & 0 \\ 0 & 0 & \dots \end{bmatrix} R^T$$

Lie groups / Lie algebras

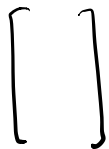
if $\lambda = 0$ an eigenvalue of K
then $e^{kt} = 1 \rightarrow$ this eigenvector is called
an axis of rotation
have to exist in odd dimensions

MATRIX INVERSES:

$A \in \mathbb{R}^{n \times m}$

assume smaller matrix dim has full rank

A tall

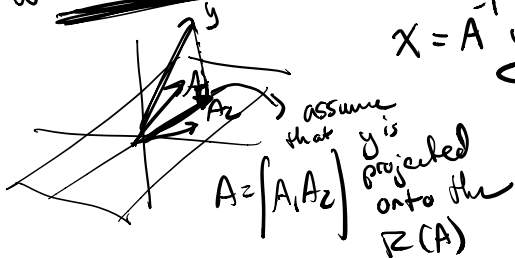


cols lin ind



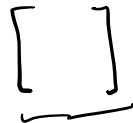
probably no solution
because likely $y \notin R(A)$

want to do our best.



$y \neq Ax$

A square



cols & rows ind

$y = Ax$
 \downarrow
unique soln

$x = A^{-1} y$

A fat



rows lin ind

continuum of solutions

A has a non-trivial nullspace $N(A)$
so if $y = Ax = A(\bar{x} + z)$

now want to x with the minimum $|x|$
so find "smallest" norm x

try to minimize ...

$$\text{set } \nabla |y - Ax|^2 = 0$$

$$\frac{d}{dx} (y^T - x^T A^T) (y - Ax)$$

$$\frac{d}{dx} (y^T - 2y^T A x + x^T A^T A x) = 0$$

$$-2y^T A + 2x^T A^T A = 0$$

$$\Rightarrow \boxed{x = (A^T A)^{-1} A^T y}$$

Least squares solution

getting x as close as possible

$$\begin{bmatrix} x \end{bmatrix} = \begin{bmatrix} A^T A \end{bmatrix}^{-1} \begin{bmatrix} A^T \end{bmatrix} \begin{bmatrix} y \end{bmatrix}$$

estimation

y : measurement signal
 x : estimate relatively bad state

spoiler:

" A " : observability matrix

$$\begin{bmatrix} \dot{y} \end{bmatrix} = \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix} x_0$$

$$y = A(\bar{x} + z) \quad z \in N(A)$$

minimize

$$|\bar{x} + z|^2 = \bar{x}^T \bar{x} + \underbrace{2z^T \bar{x} + z^T z}_{\text{useless}}$$

$$\bar{x} \in R(A^T)$$

$$z = 0$$

before domain $N(A) \oplus R(A^T)$
 nothing $\bar{x} \in R(A^T)$
 A

$$\bar{x} = A^T w$$

$$y = \underbrace{A A^T}_{\text{invertible}} w \Rightarrow w = (A A^T)^{-1} y$$

$$\boxed{\bar{x} = A^T (A A^T)^{-1} y}$$

minimum norm soln for x

$$(A A^T)^{-1}$$

$$\begin{bmatrix} x \end{bmatrix} = \begin{bmatrix} A^T \\ A \end{bmatrix} \begin{bmatrix} \\ \end{bmatrix} \begin{bmatrix} y \end{bmatrix}$$

spoiler:
 picking control signal

y : desired state
 x : control signal

multiple options for picking

spoiler:

" A " : controllability matrix

$$\underline{x_{k+1}} = A^k x_0 = [A^{n-1} B \dots A B B] \begin{bmatrix} u_0 \\ \vdots \\ u_{n-1} \end{bmatrix}$$

LTI Systems: (Linear Time Invariant) $x \in \mathbb{R}^n$

Continuous Time: $\dot{x} = Ax + Bu$
 $y = Cx$

Discrete Time: $x[t+1] = Ax[t] + Bu[t]$
 $y[t] = Cx[t]$

Solutions

$x(t) = \underbrace{e^{At}}_{\text{drift}} x(0) + \int_0^t \underbrace{e^{A(t-\tau)}}_{\text{drift}} \underbrace{Bu(\tau)}_{\text{drift}} d\tau$

$x[t] = \underbrace{A^t}_{\text{drift}} x[0] + \sum_{\tau=0}^{t-1} \underbrace{A^{t-\tau-1}}_{\text{drift}} \underbrace{Bu[\tau]}_{\text{drift}}$

Solutions

$x(t) = e^{At} x(0) + \int_0^t e^{A(t-\tau)} Bu(\tau) d\tau$

$x[t] = A^t x[0] + \sum_{\tau=0}^{t-1} A^{t-\tau-1} Bu[\tau]$

$x(t) = e^{At} x(0) + \begin{bmatrix} e^{A(t-\tau)} & B \end{bmatrix} \begin{matrix} u(0) \\ \vdots \\ u(t) \end{matrix}$

dim x dim u

continuum $[0, t]$

$x[t] = A^t x[0] + \underbrace{\begin{bmatrix} A^{t-1} & \dots & AB & B \end{bmatrix}}_{\text{cis}} \begin{bmatrix} u[0] \\ \vdots \\ u[t-1] \end{bmatrix}$

"matrix multiplication along this dim is \sum_0^t "

Controllability/Reachability

question about the range space of *

$x(t) - e^{At} x(0) \in R(\underbrace{\int_0^t e^{A(t-\tau)} B}_{\text{sloppy notation}})$

$x[t] - A^t x[0] \in R(\underbrace{\begin{bmatrix} A^{t-1} & \dots & AB & B \end{bmatrix}}_{\downarrow \text{what is the range of}})$

sloppier...

$R(\int_0^t e^{A(t-\tau)} B) = R(\begin{bmatrix} A^{n-1} & \dots & AB & B \end{bmatrix})$
 can be shown rigorously.

reason...

$e^{A(t-\tau)}$ is a polynomial in A

$R(\begin{bmatrix} A^{t-1} & \dots & AB & B \end{bmatrix}) \subseteq R(\begin{bmatrix} A^{n-1} & \dots & AB & B \end{bmatrix})$
 check.

Cayley-Hamilton: implies

that $A^t = \beta_{n-1}(t)A^{n-1} + \dots + \beta_1(t)A + \beta_0(t)I$

for any $t \geq n-1$

$\begin{bmatrix} A^{n-1} & \dots & AB & B \end{bmatrix}$

if this spans \mathbb{R}^n

Controllability matrix

\rightarrow controllable or reachable

A system is controllable iff $[A^{n-1}B \dots AB B]$ spans \mathbb{R}^n
 in both continuous & discrete time full row rank

Controllability Gramians

if M is full row rank $\iff (MM^T)$ is invertible.

$[M] \begin{bmatrix} M^T \end{bmatrix} = [] \iff$ invertible

CONTINUOUS TIME GRAMMIAN

$$W_c = \int_0^t e^{A(t-\tau)} B B^T e^{A^T(t-\tau)} d\tau$$

 rigorous

related to the unrigorous thing above

$$W_c = \begin{bmatrix} e^{A(t-\tau)} B \\ \tau \\ t \end{bmatrix} \begin{bmatrix} B^T e^{A^T(t-\tau)} \end{bmatrix}$$

not rigorous summing the inner dim is integrating...

DISCRETE TIME GRAMMIAN:

$$W_c = [A^{n-1}B \dots AB B] \begin{bmatrix} B^T \\ B^T A^T \\ \vdots \\ B^T (A^{n-1})^T \end{bmatrix}$$

 same rank

NOTE: could also use

$$W_c = [A^{t-1} B \dots AB B] \begin{bmatrix} B^T \\ B^T A^T \\ \vdots \\ B^T (A^{t-1})^T \end{bmatrix}$$

rank would be the same.

BREAK:

DYNAMICS & COORDINATE TRANSFORMS

$\dot{x} = Ax + Bu$
 $y = Cx$

want to apply new coords \implies
 $x = Tz$

$\dot{z} = ATz + Bu$
 $y = CTz$



similar for discrete time...

what happens to $[A^{n-1}B \dots AB B]$?

what is

$$[\bar{A}^{n-1} \bar{B} \dots \bar{A}B \bar{B}] = [\bar{T}^{-1}A^{n-1}\bar{T}^{-1} \dots \bar{T}^{-1}A\bar{T}^{-1} \bar{T}^{-1}B]$$

$$= \bar{T}^{-1} [A^{n-1}B \dots AB B]$$

doesn't change the row rank since T is invertible

How does controllability break?

① the vector B written in the eigen coords doesn't contain a specific eigenvector or mode

B is orthogonal to left vectors of A

② you have repeat eigenvalues and not enough inputs

③ transform into eigen coords $x = Tz$

$$\bar{B} = T^{-1}B \Rightarrow \bar{B} = \begin{bmatrix} * \\ * \\ 0 \\ * \\ * \end{bmatrix} \quad \begin{array}{l} \text{cols are} \\ \text{eigen vectors} \end{array}$$

$$\Rightarrow T\bar{B} = B$$

$$[v_1 \dots v_n] \begin{bmatrix} * \\ * \\ 0 \\ * \\ * \end{bmatrix} = v_1 \bar{B}_1 + \dots + v_{i-1} \bar{B}_{i-1} + v_{i+1} \bar{B}_{i+1} + \dots$$

$$\bar{T}^{-1}AT = D \quad [A^{n-1} \bar{B} \dots \bar{A}B \bar{B}] = [D^{n-1} \begin{bmatrix} * \\ * \\ 0 \\ * \\ * \end{bmatrix} \dots D \begin{bmatrix} * \\ * \\ 0 \\ * \\ * \end{bmatrix} \begin{bmatrix} * \\ * \\ 0 \\ * \\ * \end{bmatrix}]$$

eigen mode can't be controlled $\rightarrow = [0 \ 0 \ 0 \ 0 \ 0]$

$A = TDT^{-1}$
 directions of evolution of the sys. \rightarrow input directions $\begin{bmatrix} * \\ * \\ 0 \\ * \\ * \end{bmatrix} = T^{-1}B$

② in the eigenvector coordinates

$$[D^{-1} \bar{B} \dots D \bar{B} \bar{B}] = \begin{bmatrix} \lambda_1 & 0 & \dots & \bar{B}_1 \\ 0 & \lambda_2 & \dots & \bar{B}_2 \\ \dots & \dots & \dots & \dots \\ 0 & \dots & \dots & \bar{B}_n \end{bmatrix} \dots \begin{bmatrix} \bar{b}_1 \\ \bar{b}_2 \\ \dots \\ \bar{b}_n \end{bmatrix}$$

ratios
of the
same
always

$$\bar{B} = \begin{bmatrix} \bar{b}_1 \\ \bar{b}_2 \\ \dots \\ \bar{b}_n \end{bmatrix} \quad D = \begin{bmatrix} \lambda_1 & 0 & & 0 \\ 0 & \lambda_2 & & 0 \\ & & \dots & \\ 0 & & & \lambda_n \end{bmatrix}$$

PBH TEST:

$$[\lambda I - A \mid B] \iff \text{the system is controllable}$$

if matrix full row rank (spans \mathbb{R}^n)
for $\lambda = \lambda_1, \dots, \lambda_n$
eigenvalues

MINIMUM NORM CONTROL INPUTS:

$$\underbrace{x(t) - e^{At} x(0)}_{\text{target "y"}}$$

$$= \underbrace{\begin{bmatrix} e^{At} B \\ B \end{bmatrix}}_{\text{where we can get "A"}}$$

$$\begin{bmatrix} u(0) \\ \vdots \\ u(t) \end{bmatrix}$$

input "x"

$$x(t) - A^t x(0) = \underbrace{\begin{bmatrix} A^t B^1 & \dots & A B B \end{bmatrix}}_{\text{where we can get to "A"}}$$

$$\begin{bmatrix} u(0) \\ \vdots \\ u(t-1) \end{bmatrix}$$

input "x"

FROM BEFORE: SOLVING $y = Ax$
minimum norm solution was $x = \begin{bmatrix} A^T (AA^T)^{-1} \end{bmatrix} y$

$$y = Ax = \begin{bmatrix} A \\ A^T \end{bmatrix} \begin{bmatrix} A \\ A^T \end{bmatrix}^{-1} y = y$$

CONT. TIME MIN NORM CONT.

DISCRETE TIME MIN NORM CONT.

$$u(t) = \underline{B^T e^{A^T t} W_c^{-1}} [x(t) - e^{At} x(0)]$$

will double check.
 $W_c = \int_0^t e^{A\tau} B B^T e^{A^T \tau} d\tau$ norm vector
 $B \in \mathbb{R}^{n \times m}$ $B^T \in \mathbb{R}^{m \times n}$

$$\begin{bmatrix} u(0) \\ \vdots \\ u(t-1) \end{bmatrix} = \begin{bmatrix} B^T \\ B^T A^T \\ \vdots \\ B^T (A^T)^{t-1} \end{bmatrix} W_c^{-1} [x(t) - A^t x(0)]$$

OBSERVABILITY:

How DO WE FIGURE OUT WHAT STATE WE STARTED W $x(0)$ GIVEN A SET OF OUTPUTS $y(t)$ $[0, t]$

Measurement Eqn:

$$y = Cx \\ = [C \rightarrow] \begin{bmatrix} | \\ x \\ | \end{bmatrix}$$

DISCRETE TIME CASE:

$$x(t) = e^{At} x(0) + \begin{bmatrix} e^{At} B \\ \vdots \\ B \end{bmatrix} \begin{bmatrix} u(0) \\ \vdots \\ u(t) \end{bmatrix}$$

$$x[t] = A^t x[0] + [A^{t-1} B \dots AB B] \begin{bmatrix} u[0] \\ \vdots \\ u[t-1] \end{bmatrix}$$

$$y(t) = Cx(t) = Ce^{At} x(0) + C \begin{bmatrix} \text{---} \\ \downarrow \\ \text{know} \end{bmatrix} \begin{bmatrix} u(0) \\ \vdots \\ u(t) \end{bmatrix}$$

know know

$$y[t] = CA^t x[0] + C \begin{bmatrix} \text{---} \\ \downarrow \\ \text{know} \end{bmatrix} \begin{bmatrix} u[0] \\ \vdots \\ u[t-1] \end{bmatrix}$$

know

$$\underbrace{y(t) - C \begin{bmatrix} \text{---} \\ \vdots \\ u(t) \end{bmatrix}}_{\bar{y}(t)} = Ce^{At} x(0)$$

$$\underbrace{y[t] - C \begin{bmatrix} \text{---} \\ \vdots \\ u[t-1] \end{bmatrix}}_{\bar{y}[t]} = CA^t x[0]$$

$$\bar{y}(t) = Ce^{At} \underbrace{x(0)}_{\substack{\text{estimate} \\ \text{for initial} \\ \text{state}}}$$

$$\bar{y}[t] = CA^t \underline{x[0]}$$

$$\downarrow \\ \begin{bmatrix} \bar{y}[0] \\ \bar{y}[1] \\ \vdots \\ \bar{y}[t] \end{bmatrix} = \begin{bmatrix} Cx[0] \\ CAx[0] \\ \vdots \\ CA^t x[0] \end{bmatrix}$$

also check

$$\begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix}$$

full column rank.

similarly to control.
for continuous time

$$\begin{bmatrix} \bar{y}[0] \\ \bar{y}[1] \\ \vdots \\ \bar{y}[t] \end{bmatrix} = \begin{bmatrix} C \\ CA \\ \vdots \\ CA^t \end{bmatrix} \underline{x[0]}$$

require that $\begin{bmatrix} C \\ CA \\ \vdots \\ CA^t \end{bmatrix}$ has full column rank.

LEAST SQUARES ESTIMATE

$$\begin{bmatrix} \bar{y}[0] \\ \vdots \\ \bar{y}[t] \end{bmatrix} = \begin{bmatrix} C \\ CA \\ \vdots \\ CA^t \end{bmatrix} \underline{x[0]}$$

might not exactly lie in the range of $\begin{bmatrix} C \\ CA \\ \vdots \\ CA^t \end{bmatrix}$

tall

least squares estimate of $x[0]$ is

$$x[0] = \left(\begin{bmatrix} C^T A^0 C & \dots & (A^t)^T C \end{bmatrix} \begin{bmatrix} C \\ CA \\ \vdots \\ CA^t \end{bmatrix} \right)^{-1} \begin{bmatrix} C^T A^0 C & \dots & (A^t)^T C \end{bmatrix} \begin{bmatrix} \bar{y}[0] \\ \vdots \\ \bar{y}[t] \end{bmatrix}$$

observability matrix again Cayley Hamilton only need to check that

$$\begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix} \text{ is full column rank}$$

can estimate any initial condition the system is observable

PBH TEST: $\begin{bmatrix} C \\ \lambda I - A \end{bmatrix}$ has full column rank for $\lambda = \lambda_1, \dots, \lambda_n$ \Leftrightarrow observable

PREVIEW: NEXT WEEK LINEAR STATE FEEDBACK

choose control as linear function of the state

$$u(t) = Kx(t)$$

$$\dot{x} = Ax(t) + Bu(t) = (A + BK)x(t)$$

choose $A+BK$ to have properties that we want like specific eigenvalues } \rightarrow

STATE ESTIMATION PROBLEM:

given $y(t) \rightarrow$ estimate $x(t)$ as we go...
expected meas y meas

MODEL SYSTEM: $\dot{\hat{x}} = A\hat{x} + Bu + L(C\hat{x} - y)$

\hat{x} : model of the state

$$\dot{\hat{x}} = (A + LC)\hat{x} + Bu - Ly$$

want $\hat{x} \rightarrow x$

$x, e = x - \hat{x}$ error between model & actual state

for control use $u = K\hat{x}$ \leftarrow because we don't have access to x

$$\dot{e} = \dot{x} - \dot{\hat{x}} = Ax + Bu - A\hat{x} - Bu - L(C\hat{x} - y)$$

$$= A(x - \hat{x}) - Lc(x - e) + Ly$$

$$= Ae - Lc(x - e) + Ly$$

$$= (A + Lc)e - Lcx + Ly$$

$$\dot{e} = (A + Lc)e$$

$$y = Cx$$

$$\begin{aligned}\dot{x} &= Ax + Bu = Ax + BK\hat{x} = Ax + BK(x-e) \\ &= (A+BK)x - BKe \\ \dot{e} &= (A+LC)e\end{aligned}$$

$$\begin{bmatrix} \dot{x} \\ \dot{e} \end{bmatrix} = \begin{bmatrix} A+BK & -BK \\ 0 & A+LC \end{bmatrix} \begin{bmatrix} x \\ e \end{bmatrix} \leftarrow \begin{array}{l} \text{actual} \\ \text{sys dyn.} \\ \\ \text{error} \\ \text{dyn.} \end{array}$$

eigen values of
a block diagonal matrix
are just the eigenvalues of
each block together

Summary:

can design
K to stabilize/control
the systems

can design L
to stabilize
the error
dynamics

add $L(C\hat{x} - y)$ as an input to the error
and use $u = K\hat{x} \rightarrow$ then the error goes to 0
we stabilize the system

separation principle of estimation
& control ← works in
linear systems.