

Homework 1 Questions:

Question 1 d & e: $f: \mathbb{R}^n \rightarrow \mathbb{R}$ $\frac{\partial}{\partial x_i} \left(\frac{\partial f}{\partial x_j} \right) = \frac{\partial}{\partial x_j} \left(\frac{\partial f}{\partial x_i} \right)$

e) $\frac{\partial^2 f}{\partial x^2} = \frac{\partial}{\partial x} \frac{\partial f}{\partial x} = \frac{\partial}{\partial x} \left(\begin{bmatrix} \frac{\partial f}{\partial x_1} & \dots & \frac{\partial f}{\partial x_n} \end{bmatrix} \right)$ general.
 $= \begin{bmatrix} \frac{\partial^2 f}{\partial x_1^2} & \dots & \frac{\partial^2 f}{\partial x_1 \partial x_n} \\ \vdots & \ddots & \vdots \\ \frac{\partial^2 f}{\partial x_n \partial x_1} & \dots & \frac{\partial^2 f}{\partial x_n^2} \end{bmatrix}$

d) A is not sym.

not true that $\frac{\partial^2 f}{\partial x_i \partial x_j} \neq A_{ij}$

is equal to $\frac{\partial^2 f}{\partial x_i \partial x_j} = \frac{1}{2} (A_{ij} + A_{ji})$

Homework 2 questions:

uniqueness of eigenvectors...

$$A = P D P^{-1} = \begin{bmatrix} v_1 & \dots & v_n \end{bmatrix} \begin{bmatrix} \lambda_1 & & \\ & \ddots & \\ & & \lambda_n \end{bmatrix} \begin{bmatrix} v_1 & \dots & v_n \end{bmatrix}^{-1}$$

\uparrow $E \in \mathbb{C}^{n \times n}$ (diagonal) \uparrow $E^{-1} \in \mathbb{C}^{n \times n}$ (diagonal)

$$E = \begin{bmatrix} r_1 e^{i\phi} & & \\ & \ddots & \\ & & r_n e^{i\phi} \end{bmatrix} \quad E^{-1} = \begin{bmatrix} r_1^{-1} e^{-i\phi} & & \\ & \ddots & \\ & & r_n^{-1} e^{-i\phi} \end{bmatrix}$$

$$P E = \begin{bmatrix} r_1 v_1 e^{i\phi} & \dots & \\ & \ddots & \\ & & r_n v_n e^{i\phi} \end{bmatrix} \quad E^{-1} P^{-1} = (P E)^{-1}$$

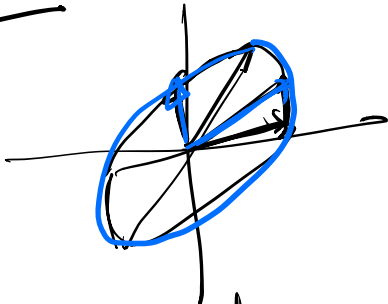
$r_1 v_1 e^{i\phi} \dots$

$$E = \begin{bmatrix} e^{i\phi} & & \\ & \ddots & \\ & & e^{-i\phi} \end{bmatrix} \propto \begin{bmatrix} c\phi & -s\phi \\ s\phi & c\phi \end{bmatrix}$$

$$\begin{bmatrix} u & v \end{bmatrix} \begin{bmatrix} c\phi - s\phi \\ s\phi & c\phi \end{bmatrix} = \begin{bmatrix} u' & v' \end{bmatrix} \quad E^{-1} = \begin{bmatrix} c\phi & -s\phi \\ s\phi & c\phi \end{bmatrix}$$

$u' = c\phi u + s\phi v$ etc.

Pictures:



Condition Number:

$$y = Ax \quad \text{A ill conditioned}$$

$$x = A^{-1}y \quad \text{essentially cols together for a particular } y, x \text{ is huge}$$

LECTURE NOTES:

Clarifications:

1) $\dot{x} = Ax + Bu \rightarrow \lambda = a + bi$ eval stability $\text{Re}(\lambda) < 0$

$x(t+1) = \bar{A}x(t) + \bar{B}u(t)$ $\bar{\lambda}$ eval \bar{A} stability $|\bar{\lambda}| < 1$

look at $\bar{A} = e^{A\Delta t}$ consistent.

$(\bar{A})^t$ if $|\bar{\lambda}_i| < 1 \quad \forall i \quad \bar{\lambda}_i^t \rightarrow 0$ if $|\bar{\lambda}_i| < 1$

2) if $M = \begin{bmatrix} A & B \\ 0 & D \end{bmatrix}$ evals $(M) = \text{evals}(A) \cup \text{evals}(D)$

evecs: $\lambda v = Av$

$\mu w = Dw$

$$M \begin{bmatrix} v \\ 0 \end{bmatrix} = \begin{bmatrix} A & B \\ 0 & D \end{bmatrix} \begin{bmatrix} v \\ 0 \end{bmatrix} = \lambda \begin{bmatrix} v \\ 0 \end{bmatrix}$$

$$M \begin{bmatrix} x \\ w \end{bmatrix} = \begin{bmatrix} A & B \\ 0 & D \end{bmatrix} \begin{bmatrix} x \\ w \end{bmatrix} = \mu \begin{bmatrix} x \\ w \end{bmatrix}$$

$\Rightarrow \mu x = Ax + Bw \Rightarrow x = (\mu I - A)^{-1} Bw$
 subtlety if μ is also eval of A
 general picture.

Interpretations of Controllability

Not controllable if

- B is tr to a left evec.

left eigenvectors =
 "input directions"

$$A = PDP^{-1}$$

$$\begin{bmatrix} A^{n-1}B & \dots & AB & B \end{bmatrix} = P \begin{bmatrix} D^{n-1}P^{-1}B & \dots & DP^{-1}B & P^{-1}B \end{bmatrix}$$

condition $\Rightarrow P^{-1}B = \begin{bmatrix} * \\ 0 \\ * \\ * \end{bmatrix} \rightarrow DP^{-1}B = \begin{bmatrix} * \\ 0 \\ * \\ * \end{bmatrix}$

$$= P \begin{matrix} \text{ith} \\ \text{entry} \end{matrix} \rightarrow \begin{bmatrix} * & \dots & * \\ 0 & 0 & 0 & 0 & 0 \\ \vdots & & & & \end{bmatrix}^n \Rightarrow \text{one the columns never shows up}$$

$$e_i^T P^{-1} P \begin{bmatrix} * \\ 0 \\ * \\ * \end{bmatrix} = [0 \dots 0]$$

\Rightarrow controllability matrix has a left nullspace

\Rightarrow not full row rank.

Transform Coords on dynamics

$$\dot{x} = Ax + Bu \quad \text{plug in } x = Tz \Rightarrow \dot{z} = T^{-1}ATz + T^{-1}Bu$$

in z coords $\left[\begin{array}{c} (T^{-1}AT)^{n-1}T^{-1}B \dots \\ (T^{-1}A^{n-1}B \dots T^{-1}ABT^{-1}B) \\ T^{-1}(A^{n-1}B \dots AB B) \end{array} \right]$

$$\left[\begin{array}{c} (T^{-1}A^{n-1}B \dots T^{-1}ABT^{-1}B) \\ T^{-1}(A^{n-1}B \dots AB B) \end{array} \right]$$

$$T^{-1} \left[\begin{array}{c} A^{n-1}B \dots AB B \end{array} \right]$$

Not observable...

$C \perp$ to a right eigenvector
"output direction"

Not controllable if

not enough inputs for repeats eigenvals.

example $\lambda_1 = \lambda_2$ $D = \begin{pmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{pmatrix}$ $\bar{B} = \mathbb{R}^{n \times 1}$

in the eigen vector coords...

$$\left[\begin{array}{c} D^{n-1} \bar{B} \dots D \bar{B} \bar{B} \end{array} \right]$$

$$\bar{B} = \begin{pmatrix} \bar{b}_1 \\ \vdots \\ \bar{b}_n \end{pmatrix} \in \mathbb{R}^2$$

if you choose $w \in \mathbb{R}^2$
st. $w^T \bar{b} = 0$

left multiply...

$$\begin{pmatrix} w^T 0 \\ \vdots \end{pmatrix} \begin{pmatrix} \lambda_1^{n-1} \bar{b}_1 & \lambda_1^{n-2} \bar{b}_1 & \dots \\ \vdots & \vdots & \dots \end{pmatrix} = \begin{pmatrix} \lambda_1^{n-1} w^T \bar{b} & \lambda_1^{n-2} w^T \bar{b} & \dots \\ 0 & \dots & 0 \end{pmatrix}$$

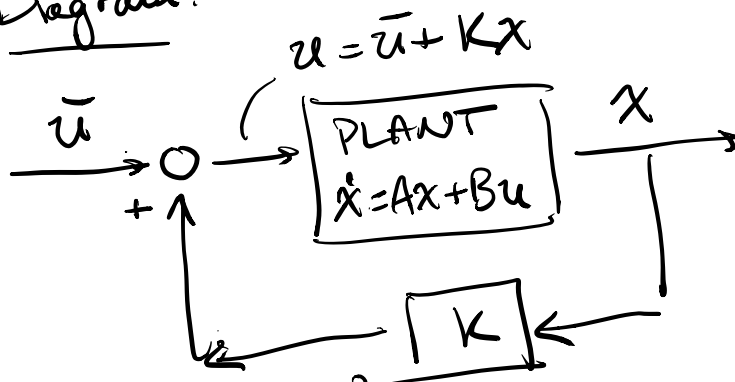
w^T can't be \perp to $\begin{pmatrix} \lambda_1^{n-1} \bar{b}_1 \\ \vdots \end{pmatrix}$ & $\begin{pmatrix} \lambda_1^{n-2} \bar{b}_1 \\ \vdots \end{pmatrix}$ etc.

if $\lambda_1 \neq \lambda_2$
 but if $\lambda_1 = \lambda_2$ then

FEEDBACK CONTROL & OBSERVER DESIGN:

$\dot{x} = Ax + Bu$ want $u = \bar{u} + Kx \Rightarrow \dot{x} = (A+BK)x + B\bar{u}$
 stable

Block Diagram:



want to shape
 evals of
 $(A+BK)$
 (eigenvectors)
 if we can

What if no access to x ?

measurement $y = Cx$ where C is not invertible

1. Model state: \hat{x}

2. Use y as input \therefore
 to the model
 dynamics
 to drive \hat{x} to x

3. use control $u = \bar{u} + k\hat{x}$

observer
design

ACTUAL STATE

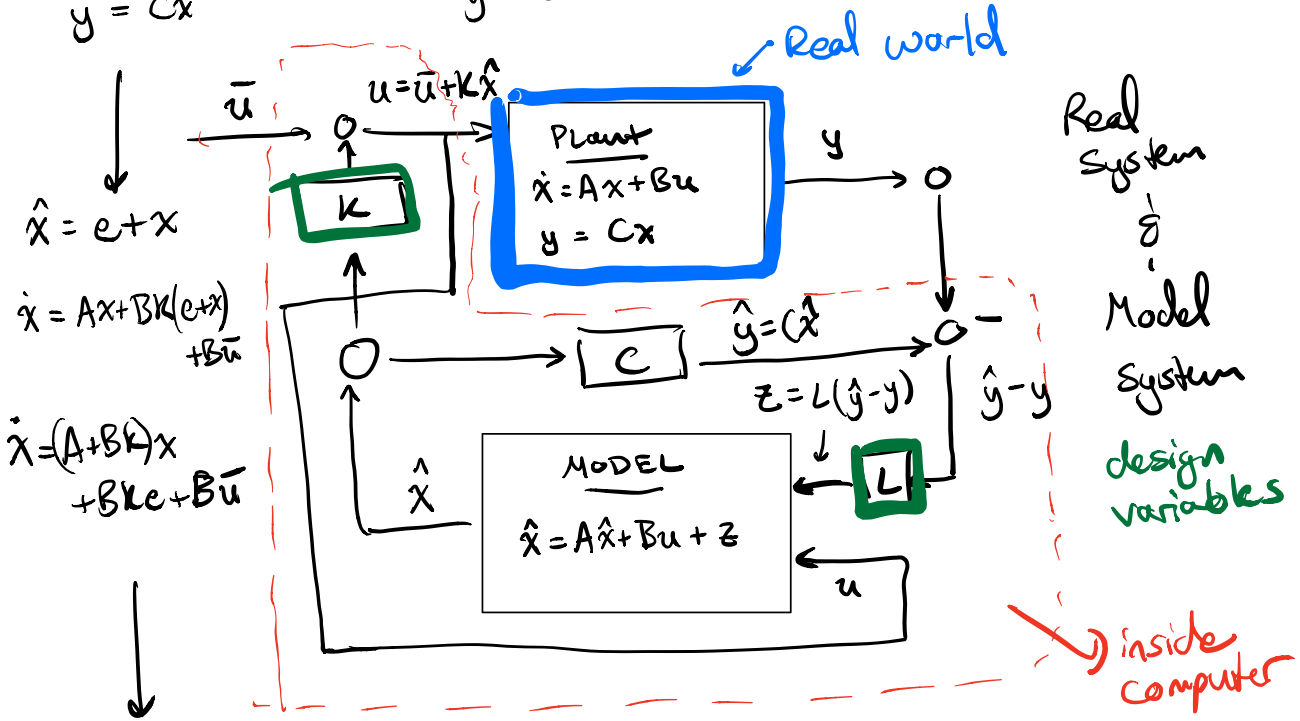
$$\begin{aligned}\dot{x} &= Ax + Bu \\ &= Ax + BK\hat{x} + B\bar{u} \\ y &= Cx\end{aligned}$$

MODEL STATE exp mess actual mess

$$\begin{aligned}\dot{\hat{x}} &= A\hat{x} + Bu + L(\hat{y} - y) \\ &= A\hat{x} + Bu + L(\hat{c}\hat{x} - Cy) \\ \hat{y} &= C\hat{x}\end{aligned}$$

ERROR DYNAMICS $e = \hat{x} - x$

$$\begin{aligned}\dot{e} &= \dot{\hat{x}} - \dot{x} = A(\hat{x} - x) + L(\hat{c}\hat{x} - Cy) \\ &= (A + LC)e\end{aligned}$$



Full Dynamics: (in terms of x & e)

$$\begin{bmatrix} \dot{x} \\ \dot{e} \end{bmatrix} = \begin{bmatrix} A+BK & BK \\ 0 & A+LC \end{bmatrix} \begin{bmatrix} x \\ e \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} \bar{u}$$

evals of this full system matrix just depend on

evals of $A+BK$
&
evals of $A+LC$

⇒ design K to stabilize $A+BK$
design L to stabilize $A+LC$ separately

⇒ separation principle

mathematically the same $A+BK \Leftrightarrow A^T+C^T L^T$

How to pick K & L :

simplest case where $B \in \mathbb{R}^{n \times 1}$ ($C \in \mathbb{R}^{1 \times n}$)

⇒ choose the evals of the closed loop system.

picking evals → choosing closed loop characteristic polynomial

want $\det(\lambda I - A - BK) = \prod_i (\lambda - \lambda_i) = \lambda^n + \beta_{n-1} \lambda^{n-1} + \dots + \beta_1 \lambda + \beta_0$

↑
design choice ↘ can compute

Assume $\det(\lambda I - A) = \lambda^n + \alpha_{n-1} \lambda^{n-1} + \dots + \alpha_1 \lambda + \alpha_0$

pick k to change char poly from given

① to ②

Consider system of form $\dot{z} = \bar{A}z + \bar{B}u$

where $\bar{A} = \begin{bmatrix} -\alpha_{n-1} & -\alpha_{n-2} & \dots & -\alpha_1 & -\alpha_0 \\ 1 & 0 & & & 0 \\ 0 & 1 & & & \\ & & \ddots & & \\ 0 & & & 1 & 0 \end{bmatrix}$ $\bar{B} = \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$

← controllable canonical form

$\det(\lambda I - \bar{A}) = \lambda^n + \alpha_{n-1} \lambda^{n-1} + \dots + \alpha_1 \lambda + \alpha_0$

if we choose $\bar{K} = [\alpha_{n-1} - \beta_{n-1} \quad \dots \quad \alpha_0 - \beta_0]$

use this gain \rightarrow closed loop
char poly is
as we want

Question:
can we find a similarity
transform that
converts our original
system to this form

$$\dot{x} = Ax + Bu$$

want T invertible
st. $x = Tz$

Answer: yes if the
system is
controllable

$$T^{-1}AT = \bar{A} \quad ; \quad T^{-1}B = \bar{B}$$

Note: $[\bar{A}^{n-1} \bar{B} \dots \bar{A} \bar{B} \bar{B}]$ is always invertible
if T exists... then we have

$$\underbrace{[\bar{A}^{n-1} \bar{B} \dots \bar{A} \bar{B} \bar{B}]}_{\bar{M}} = T^{-1} \underbrace{[A^{n-1} B \dots AB B]}_M$$

if M is invertible \leftrightarrow the system is controllable
then... $T^{-1} = \bar{M} M^{-1} \leftarrow$ similarity transform

Feedback: $Kx = KTz = \bar{K}z$

$$\Rightarrow \boxed{K = \bar{K} T^{-1} = \bar{K} \bar{M} M^{-1}}$$

- pole placement using controllable canonical form

- another version of this is Ackermann's Formula

what if $B \in \mathbb{R}^{n \times m}$?

- multiple choices for K that give the desired eigenvals \rightarrow freedom to choose eigenvectors

- place command works multi input systems. pick eigenvalues.

\rightarrow chooses eigenvectors to minimize the condition # of X where the cols of X are the eigenvectors of $A+BK$

$$X^T X = \begin{bmatrix} -x_1^T \\ \vdots \\ -x_n^T \end{bmatrix} \begin{bmatrix} | & & | \\ x_1 & \dots & x_n \\ | & & | \end{bmatrix}$$

$$= \begin{bmatrix} x_1^T x_1 & \dots & x_1^T x_n \\ \vdots & \ddots & \vdots \\ x_n^T x_1 & \dots & x_n^T x_n \end{bmatrix} \left. \vphantom{\begin{bmatrix} x_1^T x_1 & \dots & x_1^T x_n \\ \vdots & \ddots & \vdots \\ x_n^T x_1 & \dots & x_n^T x_n \end{bmatrix}} \right\} \begin{array}{l} \text{defines} \\ \text{the shape} \\ \text{of } X \end{array}$$

Polar Decomposition: if X is square invertible ...

$$X = \underbrace{X (X^T X)^{-1/2}}_{\text{ROT \& REFLECTION}} \underbrace{(X^T X)^{1/2}}_{\text{POS DEF}} = \underbrace{(X X^T)^{1/2}}_{\text{POS DEF}} \underbrace{(X X^T)^{-1/2} X}_{\text{ROT \& REFLECTION}}$$

determined by relative shape of cols

determined by relative shape of rows

like a rotation but might not have determinant of 1

like complex #s $z = r e^{i\phi}$

$$X = R P$$

rot. reflection \rightarrow pos def

Condition #

Singular Value Decomposition

For any $X \in \mathbb{C}^{n \times m}$

$$X = U \Sigma V^*$$

$U \in \mathbb{C}^{n \times n}$ $\Sigma \in \mathbb{C}^{n \times m}$

$$\begin{bmatrix} \uparrow \\ U \end{bmatrix}_n \begin{bmatrix} \overline{\Sigma} \\ 0 \\ \vdots \\ 0 \end{bmatrix}_m \begin{bmatrix} \overline{V^*} \\ \vdots \\ \vdots \end{bmatrix}_m$$

another rotation stretching first rotation

$\overline{\Sigma}$: diagonal, & positive

$$\overline{\Sigma} = \begin{bmatrix} \sigma_1 & 0 \\ 0 & \sigma_r \end{bmatrix}$$

σ_i : non zero evals of $(X^T X)^{1/2}$ & $(X X^T)^{1/2}$ or equivalently square roots of the non zero evals of $X^T X$ & $X X^T$

SVD: works on matrix of any dimension

$$X = \begin{bmatrix} u_1 & u_2 \end{bmatrix} \begin{bmatrix} \bar{\Sigma} & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} v_1^* \\ v_2^* \end{bmatrix} \Rightarrow \begin{array}{l} u_1: \text{orthonormal} \\ \text{basis for } R(X) \\ u_2: \text{orthonormal} \\ \text{basis for } N(X^*) \\ v_1: \text{orthonormal} \\ \text{basis for } R(X^*) \\ v_2: \text{orthonormal} \\ \text{basis for } N(X) \end{array}$$

Condition # $\frac{\sigma_{\max}(X)}{\sigma_{\min}(X)}$

if X is invertible:

$$X^{-1} = (U \Sigma V^*)^{-1} = V \Sigma^{-1} U^*$$

$$\Sigma^{-1} = \begin{bmatrix} \bar{\Sigma} \end{bmatrix} = \begin{bmatrix} \frac{1}{\sigma_1} & & \\ & \ddots & \\ & & \frac{1}{\sigma_k} \end{bmatrix} \text{ if } \sigma_{\max} \gg \sigma_{\min} \rightarrow \begin{bmatrix} \text{huge} \\ \times \\ \text{small} \end{bmatrix}$$

closed loop matrix

$$A + BK = X D X^{-1} \text{ if } X \text{ is poorly conditioned}$$

$$(A + BK)X(0) = X D X^{-1} X(0) = \text{relatively close to } 0$$

pick D to have evals you want the amplitude of $X^{-1}X(0)$ could be big if X is poorly conditioned.

could be huge depending on $X(0)$

← singular value then X^{-1} gets huge in certain directions

→ place command for multi input systems chooses X to be as well conditioned as possible.

“Robust Pole Assignment in Linear State Feedback (1985) Kautsky, Nichols Van Doren.”

LINEAR TIME VARYING SYSTEMS & LINEARIZATION

CONTINUOUS TIME

$$\dot{x}(t) = A(t)x(t) + B(t)u(t)$$

State transition Matrix: $e^{A(t-t_0)} \rightarrow \Phi(t, t_0)$

solution to $\dot{\Phi}(t, t_0) = A(t)\Phi(t, t_0)$
with i.c. $\Phi(t_0, t_0) = I$

- $\Phi(t, t_0) = I$
 - $\Phi(t_0, t) = \Phi^{-1}(t, t_0)$
 - $\Phi(t, t_0) = \Phi(t, t')\Phi(t', t_0)$
 - $\dot{\Phi}(t, t_0) = A(t)\Phi(t, t_0)$
- $\Phi(t, t_0)$: map between initial cond. and cond. at time t

$x(t) = \Phi(t, t_0)x(t_0)$ if no control input
with control input:

$$x(t) = \Phi(t, t_0)x(t_0) + \int_{t_0}^t \Phi(t, \tau)B(\tau)u(\tau)d\tau$$

General form for computing this is Peano-Baker series \rightarrow nested integrals
ugly.

DISCRETE TIME

$$x[t+1] = A[t]x[t] + B[t]u[t]$$

state transition matrix: $A^t \rightarrow A[t]x \dots x A[0]$

$$x[t+1] = A[t] \dots A[0]x[0] + \sum_{\tau=0}^{t-1} A[t] \dots A[\tau+1] B[\tau]u[\tau] + B[t]u[t]$$

LINEARIZATION OF NONLIN. DYN

$$\dot{x} = f(x, u, t)$$

nominal control trajectory: $\bar{u}(t)$

plug into dynamics to get nominal state trajectory: $\bar{x}(t)$

solution to integrating the dynamics

will apply control $u = \bar{u} + \Delta u = \bar{u} + K\Delta x$

addition to control to stabilize around trajectory

$$X(t) = \bar{x}(t) + \underline{\Delta X(t)}$$

perturbations
to the state

$$\dot{X} = \dot{\bar{x}} + \dot{\Delta X} = f(\bar{x} + \Delta x, \bar{u} + \Delta u, t)$$

$$\dot{\bar{x}} + \dot{\Delta X} = f(\bar{x}, \bar{u}, t) + \left. \frac{\partial f}{\partial x} \right|_{\bar{x}, \bar{u}, t} \Delta x + \left. \frac{\partial f}{\partial u} \right|_{\bar{x}, \bar{u}, t} \Delta u$$

$$\Delta \dot{X} = \left. \frac{\partial f}{\partial x} \right|_{\bar{x}, \bar{u}, t} \Delta x + \left. \frac{\partial f}{\partial u} \right|_{\bar{x}, \bar{u}, t} \Delta u \Rightarrow$$

LIN. TIME VARYING PERTURBATION DYNAMICS

$$\Delta X[t+1] = \Delta X[t] + \Delta t \left. \frac{\partial f}{\partial x} \right|_{\bar{x}, \bar{u}, t} \Delta X[t] + \Delta t \left. \frac{\partial f}{\partial u} \right|_{\bar{x}, \bar{u}, t} \Delta u[t]$$

$$= \left[I + \Delta t \left. \frac{\partial f}{\partial x} \right|_{\bar{x}, \bar{u}, t} \right] \Delta X[t] + \Delta t \left. \frac{\partial f}{\partial u} \right|_{\bar{x}, \bar{u}, t} \Delta u[t]$$

FORWARD EULER INTEGRATION.

IN THE LTI CASE:

A in continuous time $\rightarrow e^{A\Delta t}$ discrete time.

$$\left. \frac{\partial f}{\partial x} \right|_{\bar{x}, \bar{u}, t} \text{ in cont. time} \rightarrow I + \Delta t \left. \frac{\partial f}{\partial x} \right|_{\bar{x}, \bar{u}, t}$$

first terms in the Taylor exp of the state trans matrix.

LYAPUNOV STABILITY THEORY:

IDEA: define an "energy" function for a system \dot{x} then show that it decreases along trajectories of the system \rightarrow way to show stability.

used in linear systems: \dot{x} nonlinear systems \rightarrow related to linear quadratic regulator (LQR)

the cost-to-go in the LQR problem acts like a Lyapunov function

LEMMA: function $F(t)$ s.t.

$$\dot{F}(t) \leq \lambda F(t) \Rightarrow F(t) \leq e^{\lambda t} F(0)$$

PROOF: define $u(t) = e^{-\lambda t} F(t)$

take deriv. $\frac{d}{dt} u(t) = -\lambda e^{-\lambda t} F(t) + e^{-\lambda t} \dot{F}(t) \leq \underbrace{-\lambda e^{-\lambda t} F(t)}_{\text{terms cancel}} + \underbrace{\lambda e^{-\lambda t} F(t)}_{\text{terms cancel}}$

$$\dot{u}(t) \leq 0$$

$$u(t) = e^{-\lambda t} F(t) \leq u(0) = F(0)$$

$$\Rightarrow e^{-\lambda t} F(t) \leq F(0) \Rightarrow F(t) \leq e^{\lambda t} F(0)$$

if we know the derivative of a scalar function is always bounded by some scalar times the function value \rightarrow then we can use that scalar value λ as decay rate that bounds the function

\rightarrow useful when $\lambda < 0$

$$\text{because } e^{\lambda t} \rightarrow 0 \Rightarrow F(t) \rightarrow 0$$

$F(t)$: energy type function

Apply to linear systems:

Consider function $F(x(t)) = x(t)^T P x(t)$

where $P = P^T > 0$
is symmetric PD

and x evolves according to $\dot{x} = Ax$

$$\dot{F} = \frac{\partial F}{\partial x} \dot{x} = x^T P \dot{x} + \dot{x}^T P x$$

"Lie derivative" = $x^T P A x + x^T A^T P x = x^T (A^T P + P A) x$

Note: for a matrix $Q = Q^T > 0$

$$\lambda_{\min}(Q) |x|^2 \leq x^T Q x \leq \lambda_{\max}(Q) |x|^2$$

suppose $A^T P + P A = -Q$ for some $Q = Q^T > 0$

$$\dot{F}(x(t)) = -x^T Q x \leq -\lambda_{\min}(Q) |x|^2 \leq -\frac{\lambda_{\min}(Q)}{\lambda_{\max}(P)} x^T P x$$

from $\lambda_{\min}(Q) |x|^2 \leq x^T Q x$

$\frac{x^T P x}{\lambda_{\max}(P)} \leq |x|^2$

Note: the negative signs.

$$\dot{F}(x(t)) \leq \underbrace{-\frac{\lambda_{\min}(Q)}{\lambda_{\max}(P)}}_{< 0} F(t) \Rightarrow F(t) \leq e^{-\frac{\lambda_{\min}(Q)}{\lambda_{\max}(P)} t} F(0)$$

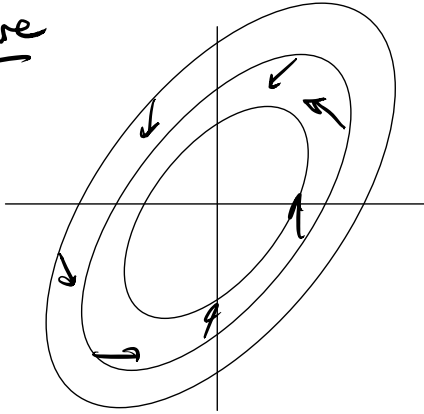
Note: $F(x(t)) = x^T P x > 0$ for $x \neq 0$

$$F(0) = 0$$

since $-\frac{\lambda_{\min}(Q)}{\lambda_{\max}(P)} < 0 \Rightarrow e^{-\frac{\lambda_{\min}(Q)}{\lambda_{\max}(P)} t} F(0) \rightarrow 0 \Rightarrow F(x(t)) \rightarrow 0$

since $F = 0$ only at $x(t) = 0 \rightarrow x(t) \rightarrow 0$

Picture



if we show \dot{x} always makes $F(x)$ decrease then we can use this to show stability.

